

# Dane County Conditional Use Permit Application

<b>Application Date</b>	<b>C.U.P Number</b>
04/08/2016	DCPCUP-2016-02343
<b>Public Hearing Date</b>	
05/24/2016	

OWNER INFORMATION		AGENT INFORMATION	
OWNER NAME DALE L STENJEM	Phone with Area Code	AGENT NAME US CELLULAR C/O WIRELESS PLANNING LLC	Phone with Area Code (414) 308-2886
BILLING ADDRESS (Number, Street) 3012 STATE HIGHWAY 134		ADDRESS (Number, Street) N64 W12883 DAYLILY COURT	
(City, State, Zip) CAMBRIDGE, WI 53523		(City, State, Zip) Menomonee Falls, WI 53051	
E-MAIL ADDRESS		E-MAIL ADDRESS Toddanderson@wirelessplanning.com	

ADDRESS/LOCATION 1		ADDRESS/LOCATION 2		ADDRESS/LOCATION 3	
ADDRESS OR LOCATION OF CUP		ADDRESS OR LOCATION OF CUP		ADDRESS OR LOCATION OF CUP	
TOWNSHIP CHRISTIANA	SECTION 1	TOWNSHIP	SECTION	TOWNSHIP	SECTION
PARCEL NUMBERS INVOLVED		PARCEL NUMBERS INVOLVED		PARCEL NUMBERS INVOLVED	
0612-014-8515-0		---		---	

CUP DESCRIPTION
195' self-support tower

DANE COUNTY CODE OF ORDINANCE SECTION	ACRES
10.194	.23

<b>DEED RESTRICTION REQUIRED?</b>  <input type="checkbox"/> Yes <input type="checkbox"/> No  Applicant Initials _____	Inspectors Initials  AMA1	SIGNATURE:(Owner or Agent)
		PRINT NAME:
		DATE:

COMMENTS: LEASE AREA IS 10,000 SQFT

Cambridge Dr station



DANE COUNTY  
PLANNING DEVELOPMENT

Zoning Division  
Room 116, City-County Building  
210 Martin Luther King Jr. Blvd.  
Madison, Wisconsin 53703-3342  
Phone: (608) 266-4266  
Fax: (608) 267-1540

Conditional Use Application

Application Fee: \$486 Mineral Extraction: \$1136

Items required to be submitted with application:

- o Written Legal Description of Conditional Use Permit boundaries
- o Scaled drawing of the property showing existing/proposed buildings, setback requirements, driveway, parking area, outside storage areas, location/type of exterior lighting, any natural features, and proposed signs.
- o Scaled map showing neighboring area land uses and zoning districts
- o Written operations plan describing the items listed below (additional items needed for mineral extraction sites)
- o Written statement on how the proposal meets the 6 standards of a Conditional Use

Owner United States Cellular operating company LLC Agent Todd Anderson  
 Address 5117 West Terrace Drive Address N64W12803 Daylily Court  
 Phone MADISON, WI 53578 Phone MENOMONIE Falls, WI 53051  
 Email \_\_\_\_\_ Phone 414-308-2886  
 Email \_\_\_\_\_ Email Todd Anderson@wirelessplanning.com

Parcel numbers affected: 0161042 - 014-8515-0 Town: CHRISTIANA Section: 1  
 Property Address: TBD Lagoon Drive

Existing/ Proposed Zoning District: A-4

- o Type of Activity proposed: Construct a 195' self-support tower
- o Hours of Operation - UN MANNED
- o Number of employees - NA
- o Anticipated customers NA
- o Outside storage - NONE
- o Outdoor activities - NONE
- o Outdoor lighting - Light on shelter
- o Outside loudspeakers - NONE
- o Proposed signs - only what is required by FAA or FCC
- o Trash removal - NA
- o Six Standards of CUP (see back)

The statements provided are true and provide an accurate depiction of the proposed land use. I authorize that I am the owner or have permission to act on behalf of the owner of the property.

Submitted By: [Signature] - Todd Anderson - Agent

Date: 3/1/16

## Six Standards of a Conditional Use Permit

Provide an explanation on how the proposed land use will meet all six standards.

1. The establishment, maintenance or operation of the conditional use will not be detrimental to or endanger the public health, safety, comfort or general welfare. *The proposed tower will not endanger the public health, safety, comfort or general welfare. Tower was sited in a location we felt would be as far from residents & still meet USCOB's coverage goals.*
2. The uses, values and enjoyment of other property in the neighborhood for purposes already permitted shall be in no foreseeable manner substantially impaired or diminished by establishment, maintenance or operation of the conditional use. *The tower should not substantially impact or diminish the area. The tower will improve coverage in the district.*
3. That the establishment of the conditional use will not impede the normal and orderly development and improvement of the surrounding property for uses permitted in the district.  
*The proposed tower will not.*
4. That adequate utilities, access roads, drainage and other necessary site improvements have been or are being made. *The proposed tower will not change drainage and utilities are at Larson Drive.*
5. Adequate measures have been or will be taken to provide ingress and egress so designed as to minimize traffic congestion in the public streets. *The proposed ingress & egress should work seeing as there is minimal traffic to the site.*
6. That the conditional use shall conform to all applicable regulations of the district in which it is located.  
*The tower will conform to all applicable regulations.*

## LEASE PARCEL

A part of the Northwest Quarter (NW1/4) of the Southeast Quarter (SE1/4) of Section One (1), Township Six (6) North, Range Twelve (12) East, Town of Christiana, Dane County, Wisconsin containing 10,000 square feet (0.229 acres) of land and being described by:

Commencing at the East Quarter Corner of said Section 1; thence  $S00^{\circ}-21'-54''W$  203.39 feet along the East line of the SE1/4 of said Section 1; thence  $N89^{\circ}-38'-06''W$  1328.14 feet to the point of beginning; thence  $S87^{\circ}-12'-38''W$  100.00 feet; thence  $N02^{\circ}-47'-22''W$  100.00 feet; thence  $N87^{\circ}-12'-38''E$  100.00 feet; thence  $S02^{\circ}-47'-22''E$  100.00 feet to the point of beginning, being subject to any and all easements and restrictions of record.

## UTILITY AND INGRESS/EGRESS EASEMENT

A part of the Northwest Quarter (NW1/4) of the Southeast Quarter (SE1/4) of Section One (1), Township Six (6) North, Range Twelve (12) East, Town of Christiana, Dane County, Wisconsin containing 5,305 square feet (0.122 acres) of land and being described by:

Commencing at the East Quarter Corner of said Section 1; thence  $S00^{\circ}-21'-54''W$  203.39 feet along the East line of the SE1/4 of said Section 1; thence  $N89^{\circ}-38'-06''W$  1328.14 feet; thence  $S87^{\circ}-12'-38''W$  100.00 feet; thence  $N02^{\circ}-47'-22''W$  100.00 feet to the point of beginning; thence  $S87^{\circ}-12'-38''W$  4.88 feet;  $N56^{\circ}-46'-36''W$  7.77 feet; thence  $S87^{\circ}-58'-42''W$  54.10 feet; thence  $N49^{\circ}-55'-54''W$  36.32 feet to a point on the South Right of Way line of Lagoon Drive; thence  $N87^{\circ}-12'-38''E$  201.88 feet along said South Right of Way line of Lagoon Drive;  $S02^{\circ}-47'-22''E$  30.00 feet; thence  $S87^{\circ}-12'-38''W$  110.00 feet to the point of beginning, being subject to any and all easements and restrictions of record.

## 10 FOOT WIDE UTILITY EASEMENT

A part of the Northwest Quarter (NW1/4) of the Southeast Quarter (SE1/4) of Section One (1), Township Six (6) North, Range Twelve (12) East, Town of Christiana, Dane County, Wisconsin containing 500 square feet (0.011 acres) of land and being described by:

Commencing at the East Quarter Corner of said Section 1; thence  $S00^{\circ}-21'-54''W$  203.39 feet along the East line of the SE1/4 of said Section 1; thence  $N89^{\circ}-38'-06''W$  1328.14 feet; thence  $N02^{\circ}-47'-22''W$  49.97 feet to the point of beginning; thence continue thence  $N02^{\circ}-47'-22''W$  50.03 feet; thence  $N87^{\circ}-12'-38''E$  10.00 feet;  $S02^{\circ}-47'-22''E$  50.03 feet; thence  $S87^{\circ}-12'-38''W$  10.00 feet to the point of beginning, being subject to any and all easements and restrictions of record.

## **MEMO**

**To:** Dane County  
**From:** Todd Anderson  
**Date:** 3/1/16  
**Re:** CTIF Exhibit E –Stenjem Property

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To whom it may concern,

United States Cellular Operating Company LLC (USCOC) is proposing to construct a 195' Self-Support tower off Lagoon Drive in the Town of Christiana, Dane County, Wisconsin. The proposed tower is being constructed will improve coverage in the area and add capacity to the existing network.

USCOC's site of choice was to collocate on the existing water tower off S.T.H. 134 and we started working with the Village on a collocation. Part of the collocation process for USCOC is to run a structural analysis on all collocation to confirm the structure will be adequate to support the proposed loading. The structural came back showing the railing on the water tank would be at 330% of capacity with their equipment, I have attached the engineer's letter and sent the County a copy of the structural. This type of an upgrade would make cost prohibitive to modify the water tank so we expanded the search to other properties in the area. We worked on trying to stay in the immediate area to meet the needs of USCOC and to also keep the tower out of the direct view of any residents.

When USCOC was looking at possible collocations in the area there was a lite guyed tower located to the east of the proposed tower near the recycling center. This tower would not have been structurally capable of supporting USCC and has since been taken down.

USCOC will send the propagation maps directly to the 3<sup>rd</sup> party engineer once we are given the information and approval from the County to send them.

Please let me know if you have any questions.

Thank you,

Todd Anderson  
Wireless Planning  
414-308-2886

**COMMUNICATION TOWER INFORMATION FORM (CTIF)**

<b>CONTACTS</b>				
Property Owner's Name		Dale & Karen Stenjem		
Property Owner's Mailing Address	3012 S.T.H. 134 <small>Street</small>	Cambridge <small>City</small>	WI <small>State</small>	53523 <small>ZIP</small>
Property Owner's Phone Number		( 608 ) 220-2232		
Agent's Name & Affiliation		Todd Anderson/ Agent for United States Cellular Operating Company LLC		
Agent's Relationship to Property Owner		Agent for USCOC		
Agent's Relationship to the Proposed Tower (e.g. wireless service provider, site acquisition firm, tower builder, etc.)		Site Acquisition Firm		
Agent's Mailing Address	N64W12883 Daylily Court <small>Street</small>	Menomonee Falls <small>City</small>	WI <small>State</small>	53051 <small>ZIP</small>
Agent's Phone Number		(414 ) 308-2886		
<b>PROPOSED ACTION</b>				
Current Zoning	A-4	CUP Acres	68	
Proposed Zoning (only if rezoning)	N/A	Rezoned Acres (if applicable)	N/A	
Have the property owner and the agent/tower sponsor formally completed a binding letter of intent, option to lease, or lease? Please attach a letter from the property owner(s) consenting to the application.			<input checked="" type="radio"/> Yes	No
			<i>Circle One</i>	
If applicable, does the lease area coincide with the proposed CUP area?			<input checked="" type="radio"/> Yes	No
			<i>Circle One</i>	
<b>LOCATION</b>				
Town		Christiana		
PLSS location (Township, Range, ¼ ¼ Section)		T. 6N, R. 12E, NW1/4 of the SE1/4 of Sec. 1		
Parcel Number(s)		016/0612-014-8515-0		
Street Address (or Proximity to Nearest Address)		TBD Lagoon Drive		
Coordinates in Decimal Degrees (00.000000 Lat., - 00.000000 Long.)		43.014875 / -89.017672		
Is the subject property located in the Height Limitation Zoning Overlay District (HLZO), roughly within three miles of the Dane County Regional Airport (check with Zoning staff)?			Yes	<input checked="" type="radio"/> No
			<i>Circle One</i>	

<b>TOWER DETAILS</b>						
Applicant's Intended Purpose of Tower (e.g. coverage, capacity, other). Explain.		Coverage and capacity in the Cambridge area. Ralph Evans was provided prop maps.				
Type of Tower (e.g. monopole, self-support lattice, guyed lattice, etc.)				Self-Support		
Above Ground Level (AGL) Height (ft.) (i.e. maximum design potential).				195'		
Base/Ground Elevation (ft.)				847'		
What is the "fall-down radius" (ft.) of the proposed tower?				70'		
Technology to be Initially Sited on the Proposed Tower (e.g. Cellular, PCS, Radio, Television, Microwave, etc.) <sup>4</sup>				Cellular		
Number & elevation (Feet AGL) of Antenna Arrays to be Accommodated		195' 1	185' 2	175' 3	165' 4	5 6
Is the primary sponsor of this tower a wireless service provider or a tower builder?		Wireless Provider		If a wireless service provider, please include FCC license number.		KNKA612
To the best of the applicant's knowledge, will this tower be lighted?		Yes	<input checked="" type="radio"/> No	If applicable, please explain in the box below to the greatest extent known in what manner the tower will be lighted.		
		Circle One				
<i>Lighting Configuration:</i>						
Are there any mitigation measures being taken to minimize the visual impact of this tower? If so, explain. Attach an additional page if necessary. The selected location was done to make the tower as least intrusive as possible to the surrounding neighbors as we could and still meet USCOC's coverage goals for the area.						
<b>PRELIMINARY INFORMATION ON OPTIONS FOR COLLOCATION<sup>5</sup></b>						
What search area radius was used to determine the location of the proposed tower?					1 mile	
Are there any existing towers or other potentially suitable structures in excess of 80 feet in height within a 1.5 mile radius? If yes, how many structures <u>total</u> are there? 1 structures. If yes, please attach map showing the location of these structures in proximity to the proposed tower.					<input checked="" type="radio"/> Yes	No
					Circle One	
Has the applicant examined each of the structures noted above to determine if an antenna array can or may be located on the structure?					<input checked="" type="radio"/> Yes	No
					Circle One	

<sup>4</sup> Note that this statement in itself does not necessarily preclude in the future the placement of alternative technologies on this structure.

<sup>5</sup> Note that more detailed information regarding options for collocation and addressing s. 10.194(2) of the Dane County Code of Ordinances is required in the *Written Statement*.

Assign a number to each of the existing structures noted above and briefly explain in the spaces below why each one will not accommodate the proposed antenna array (e.g. structurally incapable, owner unwilling to enter into a lease, etc.). Attach additional pages if necessary.		
1. Water Tank- A structural was completed and with the proposed USCOC equipment the railing failed at 330%. Structural has been submitted to the County.		
2. When we first started looking for possible structures in the area there was a lite tower located to the east of the proposed tower and that tower has been taken down since.		
3.		
4.		
<b><i>SUBJECT PROPERTY AND SURROUNDING AREA</i></b>		
What is the current, primary use of the subject property (e.g. residential, agricultural, commercial, etc.)?	Agriculture	
What are the current, primary uses of all properties adjacent to the subject property?	Agriculture Commercial Residential	
What is the current zoning of all properties adjacent to the subject property?	A-3 C0-1 A-2 Residential	
How far (in feet) is the proposed tower from the nearest structure on an adjacent property (not on subject property)? What is the current use of the structure?	960' Warehouse	
Are there any small, private airports within a 3-mile radius of the proposed tower? If yes, give the name(s) and distance(s) in the box below.	Yes	<input checked="" type="radio"/> No
	Circle One	
<i>Name(s) and Distances of Private Airports:</i>		
If applicable, have the listed private airports within a 3-mile radius of the proposed tower been notified of the petition?	Yes	No
	Circle One	

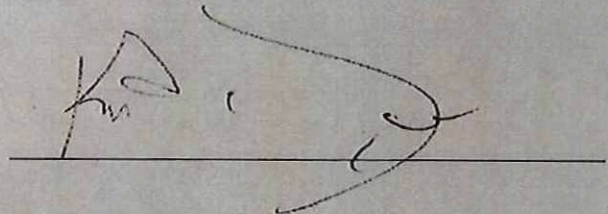


**SWORN STATEMENT OF KEN DRAKE  
IN SUPPORT OF NEW TOWER CONSTRUCTION PURSUANT TO WIS. STAT. §66.0404**

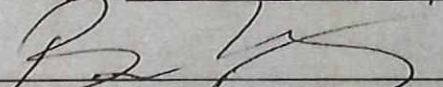
DANE COUNTY                    )  
  ) ss.  
STATE OF WISCONSIN        )

**KEN DRAKE**, being first duly sworn on oath, deposes and says that:

1. I am an adult resident of the State of Wisconsin and serve as RF Engineer at US Cellular.
2. My job duties include responsibility over the placement of the mobile service support structure being proposed at TBD Lagoon Drive, Cambridge, WI 53523 with a parcel ID number 016/0612-014-8515-0.
3. This sworn statement is made pursuant to Wis. Stat. §66.0404(2)(b)6.
4. The US Cellular proposal is being submitted because collocation within the search ring for the area covered by the proposal is infeasible as no existing structures are structurally adequate to support the proposed loading without significant modification costs which would make it no longer economically feasible to be utilized for collocation.



Subscribed and sworn to before me  
this day of March 10<sup>th</sup> 2016

  
\_\_\_\_\_  
Notary Public, State of Wisconsin  
My commission: Sept 18<sup>th</sup> 2018





624 Water Street  
Prairie du Sac, WI 53578  
608.644.1449 phone  
608.644.1549 fax

November 24, 2015

U.S. Cellular – Madison  
5117 West Terrace Drive  
Madison, WI 53718  
Contact: Mike Balistreri  
Phone: (608) 212-3808

**SUBJECT:                    STRUCTURAL ANALYSIS ADDENDUM  
                                  U.S. CELLULAR CO-LOCATION  
                                  CAMBRIDGE WT [782578]  
                                  CAMBRIDGE, WISCONSIN  
                                  EDGE PROJECT #13736**

Mr. Balistreri:

As requested from the client, we have completed a revised analysis for the above described water tower. One loading scenario was considered in the analysis. The loading condition takes into account the existing tower loading along with the proposed loading. The primary change from the previous analysis was the incorporation of the remote radios and surge arresters being mounted on the top railing. Our analysis was performed in accordance with AWWA D100-05. The analysis shows that the existing water tower is not structurally adequate to support the proposed change in loading. Based on our calculations regarding the capacity required for the water tower to sustain the proposed loading, we have concluded a structural deficiency at the tower top railing.

Loading Condition - Results		
Tower Structure Elements	Capacity Ratio (%)	Comment
Critical Section (Axial Stress w/out Wind) Top of Bell (Approx. 28' A.G.L.)	85.1%	Adequate
Critical Section (Combination Stress w/ Wind) Top of Bell (Approx. 28' A.G.L.)	88.3%	Adequate
Tower Railing (Posts)	330.0%	<b>Not Adequate</b>
Anchor Bolts (Tension)	61.9%	Adequate
Sliding	53.2%	Adequate

Although the water tower superstructure passes under proposed loading, it will be at approximately 88% capacity at its critical section. Furthermore, the addition of the existing and proposed antennas exceeds a 10% net increase in moment.

If the proposed equipment installation is altered from that which was sized, this report shall be deemed obsolete and further analysis will be required. This report is written as an addendum to the previous structural analysis by Edge Consulting Engineers. All work pertaining to the previous analysis should be considered inherently linked to this addendum work.

#### ANALYSIS REFERENCES

- Tower & foundation drawings: CB&I Eng. File: 115066 dated 7/14/2000
- Structural analysis: Edge Eng. File: 11442 dated 11/17/2014
- Tower Inventory/Site Visit: Edge Eng. File: 11442 dated 10/29/2014

Refer to the attached Cambridge WT Construction Drawings created by Edge Consulting Engineers for all applicable plan work, notes, and details.

Please feel free to contact us if you have any questions or concerns.

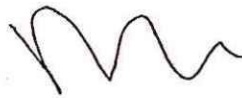
Sincerely,  
Edge Consulting Engineers, Inc.



Chris Kanne, E.I.T.  
Structural Engineer

Attachments:

- Tower Calculations
- Wind Forces on Equipment/Railing
- RAM Output
- Antenna Layout



David C. Lyshek, P.E.  
Professional Engineer



## **LIMITATIONS AND RESTRICTIONS**

1. This report was prepared in accordance with generally accepted structural engineering practices common to the telecommunication industry and makes no other warranties, either expressed or implied, as to the professional advice provided under the terms of the agreement between Engineer and Client. This report has not been prepared for uses or parties other than those specifically named, or for uses or applications other than those enumerated herein. The report may contain insufficient or inaccurate information for other purposes, applications, and/or other uses.
2. This report is intended for the use of the client, and cannot be utilized or relied upon by other parties without the written consent of Edge Consulting Engineers.
3. Edge Consulting Engineers is not responsible for any, and all, tower/building modifications completed prior to, or hereafter, which Edge Consulting Engineers was not, or will not, be directly involved.
4. The conclusions and recommendations contained within this report are based upon the supplied and attained information as described within the report. If it is known, or becomes known, that any item(s) are in conflict with what is described within this document, this report should be considered void and Edge Consulting Engineers should be contacted immediately.
5. Edge Consulting Engineers disclaims all liability for any information, conclusion, or recommendation that is not expressly stated or represented within this report.
6. Edge Consulting Engineers shall not be liable for any incidental, consequential, indirect, special, or punitive damages arising out of any claim associated with the use of this report.
7. The scope of work performed for this modification is limited to the items in which we were furnished complete and accurate information.
8. Accessories and appurtenances such as antenna mounts, feed line ladders, climbing ladders, lighting mounts, etc. were not analyzed as part of this work, and Edge Consulting Engineers, Inc. makes no claim as to their adequacy of their design or their installation.
9. This analysis was performed under the assumption that all water tower elements are in like new condition, free from rust and other deterioration. It is also assumed the tower was properly installed per construction documents, and that the tower and all associated appurtenances were originally designed and fabricated in accordance with all applicable codes and standards. Edge Consulting Engineers cannot account for, nor be held responsible, if tower elements are deteriorated, damaged, and/or missing.
10. This analysis provided by Edge Consulting Engineers, Inc. addresses the structural adequacy or deficiencies of the primary structural members. The evaluation of each bolt, plate connection detail, weld, etc. is outside the scope of this analysis.
11. This water tower analysis was performed based upon the antenna, feed line and other appurtenance loading and placement as described within this report. Any alterations to the described loading or placement will require re-analysis of the water tower, and the findings contained in this report are not valid.
12. The loading conditions utilized for this analysis is based on information provided by the client, and readily available manufacturer/vendor information (antenna and mount projected areas, weight and shape factors). However, if the described loading criteria and design assumptions within this report are not accurate, are altered, or changed in any form, this analysis shall be considered void and an additional analysis must be performed.
13. It is the responsibility of the client and the water tower owner to thoroughly review the existing and proposed loading, and bring any discrepancy to the attention of Edge Consulting Engineers.

**Wind Load Calculation**

Project Name - Cambridge WT (702670)  
 Cambridge, Wisconsin  
 Edge #19738



Completed By: CCK  
 Checked By: DCL

$P_w = q_s \cdot G \cdot C_p \cdot Z$

Where:

- $P_w$  = Wind pressure applied to horizontal projected area (lb/sq ft)
- $G$  = Gust-effect factor (1.0)
- $C_p$  = Force coefficient
- $q_s$  = Velocity pressure (lb/sq ft)

$q_s = 0.00256 K_z I V^3$

Where:

- $K_z$  = Velocity pressure exposure coefficient Exposure C
- $I$  = Wind importance factor (1.15)
- $V$  = Basic Wind Speed in mph: 90

**Force Coefficient Tables**

$C_p$ Type of Surface	$C_p$
Flat	1.00
Cylindrical or Conical with Apex Angle $\leq 15^\circ$	0.60
Double Curved or Conical with Apex Angle $\leq 15^\circ$	0.50

**Velocity Pressure Exposure Coefficient Tables**

$K_z$ Height	Exposure C	Exposure D
0 to 50 ft (15.2 m)	1.09	1.27
100 ft (30.5 m)	1.27	1.43
150 ft (45.7 m)	1.38	1.54
200 ft (61.0 m)	1.48	1.62
250 ft (76.2 m)	1.53	1.68
300 ft (91.4 m)	1.60	1.73
350 ft (106.7 m)	1.65	1.78

**Results**

Element	Area (ft <sup>2</sup> )	Z (ft)	$K_z$	$q_s$ (lb/ft <sup>2</sup> )	$C_p$	$P_w$ (lb/ft <sup>2</sup> )	$P_w$ min (lb/ft <sup>2</sup> )	$p$ (lb/ft)	Weight (lb)	O.T.M. (ft-lb)
<b>Water Tower Sections</b>										
Tank Top	1322.86	128.34	1.33	31.67	0.50	15.83	15.00	20.95		2646.11
Tank Bottom	351.10	107.65	1.29	30.85	0.00	18.39	18.00	6.46	691.30	
Upper Knuckle	50.60	97.47	1.29	30.07	0.50	15.03	15.00	0.78	74.15	
Shell Top	485.00	71.10	1.11	27.80	0.50	13.90	13.00	4.73	620.70	
Shell Bottom	193.85	37.53	1.09	25.99	0.00	15.60	15.00	3.48	130.82	
Lever Knuckle	13.28	27.31	1.09	25.99	0.50	13.00	13.00	0.20	5.43	
Top Pedestal	111.03	22.08	1.09	25.99	0.00	15.60	15.00	2.00	44.09	
Mid Pedestal	150.77	13.47	1.09	25.99	0.00	15.60	15.00	2.71	36.56	
Bot Pedestal	190.75	4.85	1.09	25.99	0.00	15.60	15.00	3.43	15.89	
<b>Railing Sections &amp; Misc.</b>										
Top Rail Horizontal (Front)	2.375	147.00	1.37	32.75	1.00	32.75	30.00	0.68		11.43
Top Rail Horizontal (Back)	1.188	147.00	1.37	32.75	1.00	32.75	30.00	0.64		5.72
Middle Rail Horizontal (Front)	3.125	145.25	1.37	32.66	1.00	32.66	30.00	0.10		14.82
Middle Rail Horizontal (Back)	1.563	145.25	1.37	32.66	1.00	32.66	30.00	0.65		7.41
Kick Plate (Front)	5.000	143.50	1.37	32.57	1.00	32.57	30.00	0.18		23.37
Kick Plate (Back)	2.500	143.50	1.37	32.57	1.00	32.57	30.00	0.68		11.65
Existing Rail Posts	4.375	145.25	1.37	32.66	1.00	32.66	30.00	0.14		23.75
<b>Existing Antennas &amp; Mount Posts</b>										
(1) Perceonics P05-16-3L-M (Existing)	18.000	143.17	1.35	32.81	1.00	32.81	30.00	0.59	132.00	87.51
(1) Jaybeam PCSA090-19-x (Existing)	23.656	143.29	1.35	32.82	0.00	19.69	18.00	0.58	143.40	64.69
(1) CSS DBC-7CAP (Existing)	3.065	143.29	1.35	32.82	1.00	32.82	30.00	0.10	48.00	14.92
(1) Mast Pipe - 8 ft 2" Std (Existing)	14.250	147.50	1.37	32.78	0.60	19.67	18.00	0.28	263.52	41.34
(1) RFI BM4040-41-DN (Existing)	8.900	157.00	1.39	33.18	0.60	19.91	18.00	0.18	68.00	27.81
(1) Mast Pipe - 5 ft 2" Std (Existing)	0.990	148.00	1.37	32.70	0.60	19.62	18.00	0.02	15.30	2.83
(1) Mast Pipe - 5 ft 2" Std (Existing)	4.604	157.00	1.39	33.18	0.60	19.91	18.00	0.09	40.00	14.30
(1) Mast Pipe - 5 ft 2" Std (Existing)	0.990	148.00	1.37	32.70	0.60	19.62	18.00	0.02	18.30	2.83
(1) COH98 (Pacific Wireless) (Existing)	3.444	156.00	1.39	33.14	1.00	33.14	30.00	0.11	26.60	17.81
(1) Mast Pipe - 10 ft 2" Std (Existing)	1.978	147.00	1.37	32.75	0.60	19.65	18.00	0.04	36.60	5.72
(1) 8" Vsgl (Existing)	1.000	147.00	1.37	32.75	0.60	19.65	18.00	0.02	10.00	2.69
(1) 4" Omni (Existing)	0.697	153.00	1.38	33.02	0.60	19.61	18.00	0.02	15.50	2.83
(1) Ubiquiti Rocket M2 (Existing)	0.140	155.00	1.39	33.10	1.00	33.10	30.00	0.00	1.10	0.72
(1) Mast Pipe - 10 ft 2" Std (Existing)	1.978	148.00	1.39	32.80	0.60	19.63	18.00	0.04	36.60	5.77
(1) 8" Omni (Existing)	1.300	157.00	1.39	33.18	0.60	19.91	18.00	0.03	24.00	4.06
(1) Mast Pipe - 10 ft 2" Std (Existing)	1.978	148.50	1.38	32.83	0.60	19.70	18.00	0.04	36.60	5.79
(1) Dish 18" (Existing)	1.398	148.00	1.38	32.80	1.00	32.80	30.00	0.05	25.00	6.78
(1) Dish 18" (Existing)	1.398	145.25	1.37	32.66	1.00	32.66	30.00	0.05	25.00	6.62
(1) Beacon (Small) (Existing)	0.250	145.25	1.37	32.66	1.00	32.66	30.00	0.01	50.00	1.19
<b>Proposed Antennas &amp; Mount Posts</b>										
(1) Kathrein 800 1C105 (Proposed)	37.121	149.50	1.38	32.88	1.00	32.88	30.00	1.22	310.80	192.43
(1) KMW KASCTP282008 (Proposed)	0.209	149.50	1.38	32.88	1.00	32.88	30.00	0.01	3.95	1.03
(1) KaXu D800056F1Vx-1 (Proposed)	2.067	149.50	1.38	32.88	1.00	32.88	30.00	0.07	30.60	10.16
(1) Ericsson RRU511 (Proposed)	20.931	149.50	1.38	32.88	1.00	32.88	30.00	0.69	458.00	102.69
(1) Raycap RUSDC-6297-4P-48 (Proposed)	5.408	149.50	1.38	32.88	1.00	32.88	30.00	0.18	47.00	28.56

Original Tower Overturning Moment = 495.84 kip-ft  
 Existing Tower Overturning Moment = 489.32 kip-ft Percent Change = 18.16  
 Proposed Tower Overturning Moment = 502.46 kip-ft Percent Change = 17.74

Note: All Percent Changes taken in relation to the Original Tower Overturning Moment

Typically an increase less than 10% in overturning results in having little effect on the adequacy of the structure.

**Critical Section Calculations**

Project Name - Cambridge WT (702570)  
 Cambridge, Wisconsin  
 Edge #13738



Completed By: CCK  
 Checked By: DCL

**Actual Stresses at the Critical Section (Top of Bell):**

Height to the Critical Section = 27.95 ft  
 Critical Section Thickness (t) = 0.6375 in  
 Shaft Height (H<sub>SA</sub>) = 605.752 in  
 Outer Diameter of Critical Section (D<sub>CO</sub>) = 121.375 in  
 Inner Diameter of Critical Section (D<sub>CI</sub>) = 120 in  
 Effective Radius (R<sub>EO</sub>) = 60.34375 in  
 r = 42.67 in  
 k = 2.00  
 K<sub>L</sub> = 37.77  
 I<sub>R</sub> = 0.01139

\*The thickness was taken from Chicago Bridge & Iron plans

Water Weight = 3391600 lb  
 Original Metal Weight = 222900 lb  
 Bell Weight = 0 lb  
 Total Proposed Equipment Weight = 1871.83 lb

\*Includes Bell Weight  
 \*Assumed to be Zero

Total Proposed Weight Above the Critical Section = 3516372 lb

Element	Area (ft <sup>2</sup> )	Z <sub>Centroid</sub> (ft)	K <sub>y</sub>	q <sub>y</sub> (lb/ft <sup>2</sup> )	C <sub>y</sub>	P <sub>w</sub> (lb/ft)	P <sub>w min</sub> (lb/ft)	p (ft/ft)	M <sub>Centroid</sub> (kip-ft)
<b>Water Tower Sections</b>									
Tank Top	1322.660	53.33	1.33	31.87	0.50	15.83	15.00	20.55	2060.48
Tank Bottom	351.100	79.09	1.29	33.65	0.50	16.39	18.00	6.46	510.74
Upper Knuckle	50.600	69.51	1.26	30.07	0.50	15.03	15.00	0.76	52.88
Shaft Top	455.000	43.14	1.17	27.60	0.50	13.80	18.00	8.73	376.61
Shaft Bottom	193.650	9.57	1.09	25.99	0.50	13.00	18.00	3.49	33.36
Lower Knuckle	13.260	-0.66	1.09	25.99	0.50	13.00	15.00	0.20	0.00
Bot Pedestal	190.760	-23.10	1.09	25.99	0.50	13.00	18.00	3.43	0.00
<b>Railing Sections</b>									
Existing Top Rail Horizontal (Front)	2.375	119.04	1.37	32.75	1.00	32.75	30.00	0.08	9.26
Top Rail Horizontal (Back)	1.188	119.04	1.37	32.75	1.00	32.75	30.00	0.04	4.63
Middle Rail Horizontal (Front)	3.125	117.29	1.37	32.66	1.00	32.66	30.00	0.10	11.97
Middle Rail Horizontal (Back)	1.563	117.29	1.37	32.66	1.00	32.66	30.00	0.05	5.99
Kick Plate (Front)	5.000	115.54	1.37	32.57	1.00	32.57	30.00	0.16	18.81
Kick Plate (Back)	2.500	115.54	1.37	32.57	1.00	32.57	30.00	0.08	9.41
Existing Rail Posts	4.375	117.29	1.37	32.66	1.00	32.66	30.00	0.14	16.76
<b>Existing Antennas &amp; Mount Pipes</b>									
(3) Powerwave P65-16XLM (Existing)	18.000	120.21	1.38	32.81	1.00	32.81	30.00	0.59	71.00
(5) Jay beam PCSA950-19x (Existing)	29.658	120.33	1.38	32.82	0.50	19.69	18.00	0.53	70.34
(5) CSS DBC-7CAP (Existing)	3.055	120.33	1.38	32.82	1.00	32.82	30.00	0.10	12.11
(2) Mast Pipe - 8 ft 2" Sld (Existing)	14.250	119.54	1.37	32.78	0.50	19.67	18.00	0.28	33.50
(1) RFI BA4040-41-D-N (Existing)	8.900	129.04	1.39	33.18	0.50	19.91	18.00	0.18	22.66
(1) Mast Pipe - 5 ft 2" Sld (Existing)	0.990	118.04	1.37	32.70	0.50	19.62	18.00	0.02	2.29
(1) 20' Dipole (Existing)	4.604	129.04	1.39	33.18	0.50	19.91	18.00	0.09	11.83
(1) Mast Pipe - 5 ft 2" Sld (Existing)	0.990	118.04	1.37	32.70	0.50	19.62	18.00	0.02	2.29
(1) OOH-9 (Pole/Wireless) (Existing)	3.444	128.04	1.39	33.14	1.00	33.14	30.00	0.11	14.61
(1) Mast Pipe - 10 ft 2" Sld (Existing)	1.979	119.04	1.37	32.75	0.50	19.65	18.00	0.04	4.63
(1) E Yagi (Existing)	1.000	119.04	1.37	32.75	0.50	19.65	18.00	0.02	2.34
(1) 4 Omni (Existing)	0.657	125.04	1.38	33.02	0.50	19.81	18.00	0.02	2.15
(1) Ubiquiti Rocket M2 (Existing)	0.140	127.04	1.39	33.10	1.00	33.10	30.00	0.00	0.59
(1) Mast Pipe - 10 ft 2" Sld (Existing)	1.979	120.54	1.38	32.83	0.50	19.70	18.00	0.04	4.70
(1) Dish 16" (Existing)	1.396	120.04	1.38	32.80	1.00	32.80	30.00	0.05	5.50
(2) Beacon (Small) (Existing)	0.250	117.29	1.37	32.66	1.00	32.66	30.00	0.01	0.98
<b>Proposed Antennas &amp; Mount Pipes</b>									
(6) Kathrein 600 10765 (Proposed)	37.121	121.64	1.38	32.83	1.00	32.83	30.00	1.22	148.35
(3) KMW KASCTFR82008 (Proposed)	0.209	121.54	1.38	32.83	1.00	32.83	30.00	0.01	0.83
(6) Kathus DBC0066F1V-1 (Proposed)	2.067	121.54	1.38	32.83	1.00	32.83	30.00	0.07	8.26
(9) Ericsson RRUs11 (Proposed)	20.931	121.54	1.38	32.83	1.00	32.83	30.00	0.69	83.65
(2) Raycap RUSDC-6267-PF-48 (Proposed)	5.428	121.54	1.38	32.83	1.00	32.83	30.00	0.18	21.61

Proposed Tower Critical Moment = 3635.29 kip-ft  
 Proposed Actual Axial Stress (f) = 13873.57 lb/in<sup>2</sup>  
 Proposed Actual Bending Stress (f) = 5546.69 lb/in<sup>2</sup>

**Allowable Stresses at the Critical Section:**

Material Class = 2  
 \*Assumed Class 2 material (F<sub>y</sub> > 34 ksi)

Allowable Compressive Stress (F<sub>c</sub>) = 17019.25 lb/in<sup>2</sup>  
 C<sub>c</sub> = 129.63  
 Reduction Factor (K<sub>f</sub>) = 0.9576

Allowable Axial Stress (F<sub>a</sub>) = 16297.53 lb/in<sup>2</sup>  
 Allowable Bending Stress (F<sub>b</sub>) = 17019.25 lb/in<sup>2</sup>

**Stresses Due to Proposed Axial Load and Bending Moment Check:**

Axial Stress w/out Wind Check = 0.851 < 1 **OK**  
 Combination Stress w/ Wind = 0.833 < 1 **OK**

**Anchorage and Sliding Check**

Project Name - Cambridge WT (782678)  
 Cambridge, Wisconsin  
 Edge #13736



Completed By: CCK  
 Checked By: DCL

**Anchorage Check:**

Number of Anchor Rods = 16  
 Diameter of Anchor Rod = .2 in  
 Area of Anchor Rod = 3.14 in<sup>2</sup>  
 Diameter of the Anchor Circle = 24.75 ft  
 Rod Yield Stress (F<sub>y</sub>) = 36 ksi  
 Rod Tensile Strength (F<sub>t</sub>) = 58 ksi  
 Original Metal Weight = 222900 lb  
 Proposed Metal Weight = 224772 lb  
 Proposed Tower Overturning Moment = 5022.46 kip-ft

\*Number of bolts taken from Chicago Bridge & Iron plans  
 \*Bolt diameter taken from Chicago Bridge & Iron plans

\*These values come from the wind load calculation sheet

**Sliding Check:**

$\mu = 0.45$   
 Proposed Resisting Shear = 101.15 kip  
 Proposed Base Shear = 53.60 kip  
 Proposed Shear Ratio = 0.532

\*Steel-to-Concrete

OK

No provisions for resisting shear are required

**Anchor Bolt Capacity:**

**Shear Checks:**

Proposed Applied Shear per Rod (V<sub>rod</sub>) = 3.35 kip/rod  
 Allowable Shear per Rod (R<sub>v</sub>/t) = 38.4 kip/rod  
 Proposed Unity = 0.092

**Tension Check**

$$T_{max} = \frac{4 \cdot M}{N_b \cdot D_{circle}} + \frac{0.6 \cdot W}{N_b}$$

Proposed Applied Tension per Rod (T<sub>rod</sub>) = 42.30 kip/rod  
 Proposed Allowable Tension per Rod (R<sub>t</sub>/t) = 68.33 kip/rod  
 Proposed Unity = 0.619

OK

## Equations

Project Name - Cambridge WT (782578)  
Cambridge, Wisconsin  
Edge #13738



Completed By: CCK  
Checked By: DCL

### Critical Section Calculation Equations:

$$D_{in} = D_{out} - 2t$$

t = Shaft Thickness

$$R_{eff} = \frac{D_{out} - t}{2}$$

$$r = \frac{\sqrt{D_{out}^2 + D_{in}^2}}{4}$$

$$\frac{KL}{r} = \frac{2 \cdot H_{shaft}}{r}$$

H<sub>shaft</sub> = Shaft Height

### Actual Stress Calculation Equations:

$$f_a = \frac{W_{exp\_total\_total}}{2 \cdot \pi \cdot R_{eff} \cdot t}$$

W<sub>exp\\_total\\_total</sub> = Total Weight Above the Critical Section

$$f_b = \frac{M_{exp\_total\_total}}{\pi \cdot R_{eff}^2 \cdot t}$$

M<sub>exp\\_total\\_total</sub> = Total Moment at the Critical Section

$$F_L = IF \left( \frac{t}{R_{eff}} \geq 0.0125, 18000 \text{ psi}, \left( 6925 + 886000 \left( \frac{t}{R_{eff}} \right) \right) \text{ psi} \right)$$

$$C'_c = \sqrt{\frac{\pi^2 \cdot E}{F_L}} \quad (\text{AWWA Eq 3-10 p 26})$$

$$K_\phi = 1.0 : \left( \frac{KL}{r} \leq 25 \right)$$

$$K_\phi = 0.5 \cdot \left( \frac{C'_c}{\frac{KL}{r}} \right)^2 : \left( \frac{KL}{r} \geq C'_c \right) \quad (\text{AWWA Eq 3-7, 3-8, 3-9 p 26})$$

$$K_\phi = 1 - 0.5 \cdot \left( \frac{\frac{KL}{r}}{C'_c} \right)^2 : \left( 25 \leq \frac{KL}{r} \leq C'_c \right)$$

$$F_a = F_L \cdot K_\phi \quad (\text{AWWA Eq 3-4 p 26})$$

$$F_b = F_L \quad (\text{AWWA Eq 3-5 p 26})$$

### Axial Load & Bending Moment Stress Checker:

Axial Stress without Wind

$$\frac{f_a}{F_a} \leq 1$$

Combination Stress with Wind

$$\frac{f_a}{F_a \cdot 1.33} + \frac{f_b}{F_b \cdot 1.33} \leq 1$$



**Equations**

Project Name - Cambridge WT (782678)  
 Cambridge, Wisconsin  
 Edge #13738



Completed By: CCK  
 Checked By: DCL

**Anchorage Check:**

Metal Weight (W) =  $W_{top} + W_{wt} + W_{shells}$

**Sliding Check:**

Resisting Shear:

$$V_{resisting} = \mu \cdot W'$$

Base Shear: (Sum of the p values in the Wind Load Table)

**Shear Check (AISC\_ABD):**

Applied Shear per Rod:

$$V_{actual} = \frac{V_{shear}}{N_s}$$

$N_s$  = Number of Anchor Rods

Allowable Shear per Rod:

$$\frac{R_n}{\Omega} = \frac{0.4 \cdot F_u \cdot A_g}{2.0}$$

Unity of Shear:

$$Unity = \frac{V_{actual}}{\frac{R_n}{\Omega}}$$

**Tension Check (AISC\_ABD):**

Applied Tension per Rod:

$$T_{actual} = \frac{A \cdot M}{N_s \cdot D_{circle}} = \frac{0.6 \cdot W}{N_s}$$

M = Tower Overturning Moment at the Top of the Footing

Allowable Tension per Rod:

$$\frac{R_n}{\Omega} = \frac{0.75 \cdot F_u \cdot A_g}{2.0}$$

Unity of Tension:

$$Unity = \frac{T_{actual}}{\frac{R_n}{\Omega}}$$

**Combined Shear and Tension Check (AISC\_ABD):**

$$OK \text{ if true } \left\{ \begin{array}{l} \frac{V_u}{R_n/\Omega} \leq 0.2 \text{ and } \frac{T_u}{R_n/\Omega} \leq 1 \\ \frac{V_u}{R_n/\Omega} \leq 1 \text{ and } \frac{T_u}{R_n/\Omega} \leq 0.2 \\ \frac{V_u}{R_n/\Omega} \leq 1 \text{ and } \frac{T_u}{R_n/\Omega} \leq 1 \text{ plus } \frac{V_u}{R_n/\Omega} + \frac{T_u}{R_n/\Omega} \leq 1.3 \end{array} \right.$$

## Water Tower Bearing Capacity Calculations:

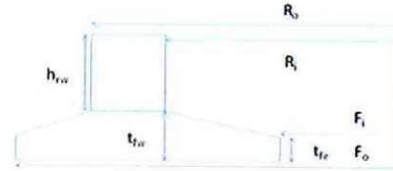
Project Name - Cambridge WT (782578)  
 Cambridge, Wisconsin  
 Edge #13738



Completed By: CCK  
 Checked By: DCL

### Foundation Dimensions & Soil Properties:

Inner Radius of Footing (F <sub>i</sub> ) =	1.75	ft
Outer Radius of Footing (F <sub>o</sub> ) =	20.00	ft
Ringwall Height Above Footing (h <sub>rw</sub> ) =	8.75	ft
Inner Radius of Ringwall (R <sub>i</sub> ) =	11.50	ft
Outer Radius of Ringwall (R <sub>o</sub> ) =	13.33	ft
Thickness of Footing at Edge (t <sub>fe</sub> ) =	0.83	ft
Thickness of Footing at Ringwall (t <sub>fw</sub> ) =	2.00	ft
Exposed Height (h <sub>e</sub> ) =	0.50	ft
Area of Foundation (A) =	1247.02	ft <sup>2</sup>
Section Modulus of Foundation (S) =	6282.82	ft <sup>3</sup>
Y <sub>soil</sub> =	100.00	lb/ft <sup>3</sup>
Y <sub>concrete</sub> =	44.00	lb/ft <sup>3</sup>
Y <sub>water</sub> =	144.00	lb/ft <sup>3</sup>



\*Assumed  
 \*Per ANSI/AWWA D100-05

### Applied Loads:

Original Tank Weight =	222.90	kip
Proposed Tank Weight =	224.77	kip
Water Weight =	3391.60	kip
Total Foundation Concrete Weight =	137.82	kip
Snow Weight =	26.13	kip
Soil Weight Applied on Foundation =	972.12	kip
Total Original Net Loads on Foundation (P <sub>net</sub> ) =	3778.45	kip
Total Proposed Net Loads on Foundation (P <sub>net</sub> ) =	3780.32	kip
Total Original Ultimate Loads on Foundation (P <sub>max</sub> ) =	5063.79	kip
Total Proposed Ultimate Loads on Foundation (P <sub>max</sub> ) =	5065.66	kip
Total Proposed Ultimate Loads on Foundation less Water (P <sub>ult</sub> ) =	1674.06	kip
Original Moment Applied at the Top of Foundation (M) =	4265.84	kip-ft
Proposed Moment Applied at the Top of Foundation (M) =	5022.46	kip-ft
Original Shear Applied at the Top of Foundation (V) =	48.72	kip
Proposed Shear Applied at the Top of Foundation (V) =	53.80	kip
Original Moment Applied at the Base of Foundation (M) =	4789.63	kip-ft
Proposed Moment Applied at the Base of Foundation (M) =	5600.86	kip-ft

### Bearing Check:

Limiting eccentricity (e) =	5.04	ft
e <sub>net</sub> =	0.95	ft
e <sub>net</sub> ' =	1.11	ft
$q_{net} = \left( \frac{P_{net}}{A} + \frac{M}{S} \right)$	q <sub>net</sub> = 3792.33	psf
	q <sub>net</sub> ' = 3922.95	psf
Percentage Change in Bearing =	3.44	%
Required ultimate net bearing pressure =	11768.85	psf

#### With Wind Increase with Water

$q_{ult\omega S} = \left( \frac{P_{net}}{A} + \frac{1.5M}{S} \right)$	e <sub>ult</sub> ' = 1.66	ft
	q <sub>ult</sub> ' = 4374.41	psf

OK - Required Bearing Capacity for Lesser Wind Condition Controls

#### With Wind Increase without Water

e <sub>ult</sub> ' =	5.02	ft
q <sub>ult</sub> ' =	1654.64	psf

OK - Required Bearing Capacity for Lesser Wind Condition Controls

### Stability Check:

Original Minimum Restoring Moment =	30164.83	kip-ft
Original F.S. for Overturning =	6.30	
Proposed Restoring Moment without Water =	30202.27	kip-ft
Proposed F.S. for Overturning =	5.39	
Proposed Restoring Moment with Water =	98034.27	kip-ft
Proposed F.S. for Overturning =	17.50	

### Antenna Wind Load Calculations

Project Name - Cambridge WT (702870)  
 Cambridge, Wisconsin  
 Edge #13738



Completed By: CSH  
 Checked By: KTS

#### Basic Wind Pressure Calculations:

Elevation of Antennas (h) = 149.17 ft  
 Exposure Category = C  
 $K_z = 1.33$   
 $V = 90$  mph  
 $I = 1.15$   
 $q_z = 0.00256 \cdot K_z \cdot V^2 \cdot I$   
 $q_z = 32.83$  psf

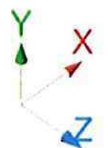
#### Wind Force/Weight Calculations:

#	Appearance	Type	Normal Orientation	Position	Weight (P) lbs	Bracket lbs	Height (H) in	Width (W) in	Depth (D) in	Front (C <sub>d</sub> )	Side (C <sub>s</sub> )	EPA <sub>front</sub> ft <sup>2</sup>	EPA <sub>side</sub> ft <sup>2</sup>	Total Weight lbs
6	Kathrein 800 10765	Antenna	Front	1	58.40	13.00	95.00	11.83	6.00	1.00	1.00	7.87	4.00	71.40
3	Eriksen RRU11 (Double-Up)	RRU	Front	2	102.00	N/A	19.70	17.00	14.40	1.00	1.00	2.33	1.97	102.00
3	Eriksen RRU11	RRU	Front	3	51.00	N/A	19.70	17.00	7.20	1.00	1.00	2.33	0.99	51.00
2	Ryejet RUSDC-6257-PF-48	Surge Arrester	Front	4	20.00	N/A	20.60	18.50	5.80	1.00	1.00	2.704	0.83	20.00

#### Summation of Wind Force:

$$F = q_z \cdot C_f \cdot A$$

Antenna Designation	1	2	3	4
Normal Force on Antenna	253.3	75.4	75.4	83.8
Tangential Force on Antenna	131.3	64.7	32.3	27.2
Total Weight	71.4	102.0	51.0	20.0





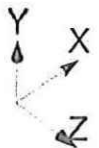
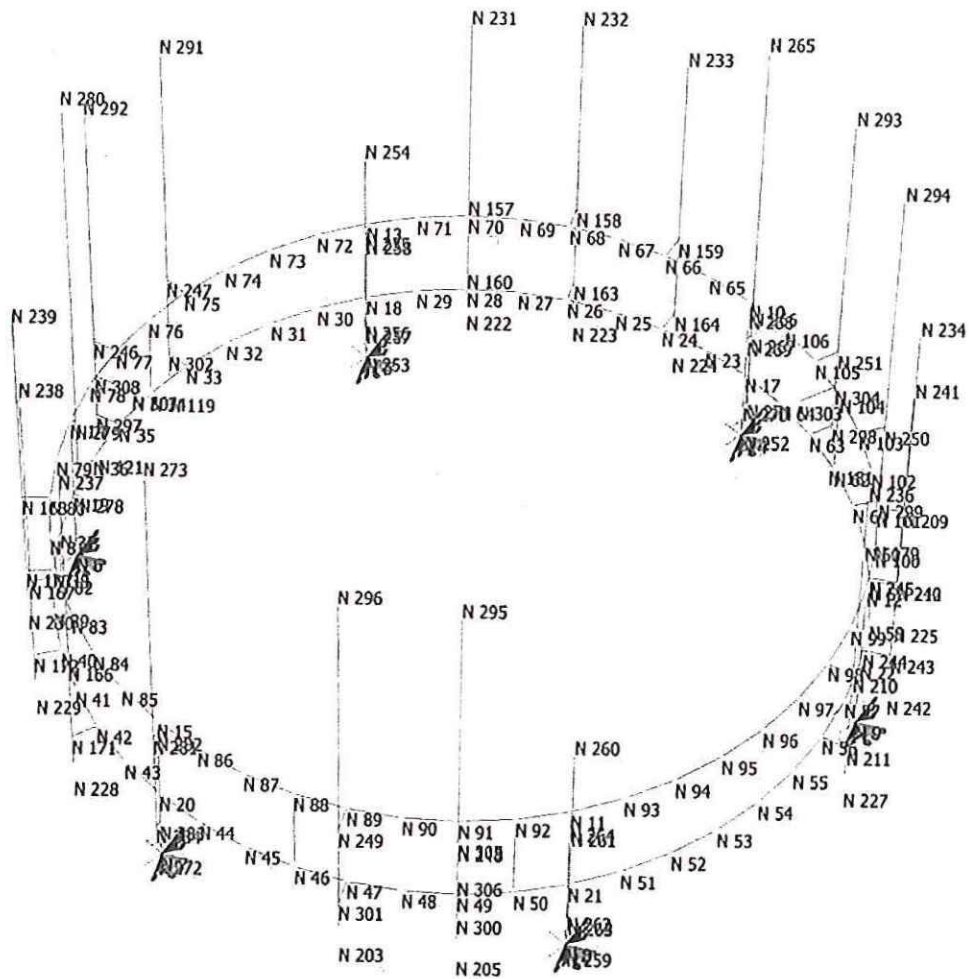
# Edge

Consulting Engineers, Inc. Edge Consulting Engineers, Inc

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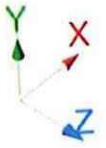
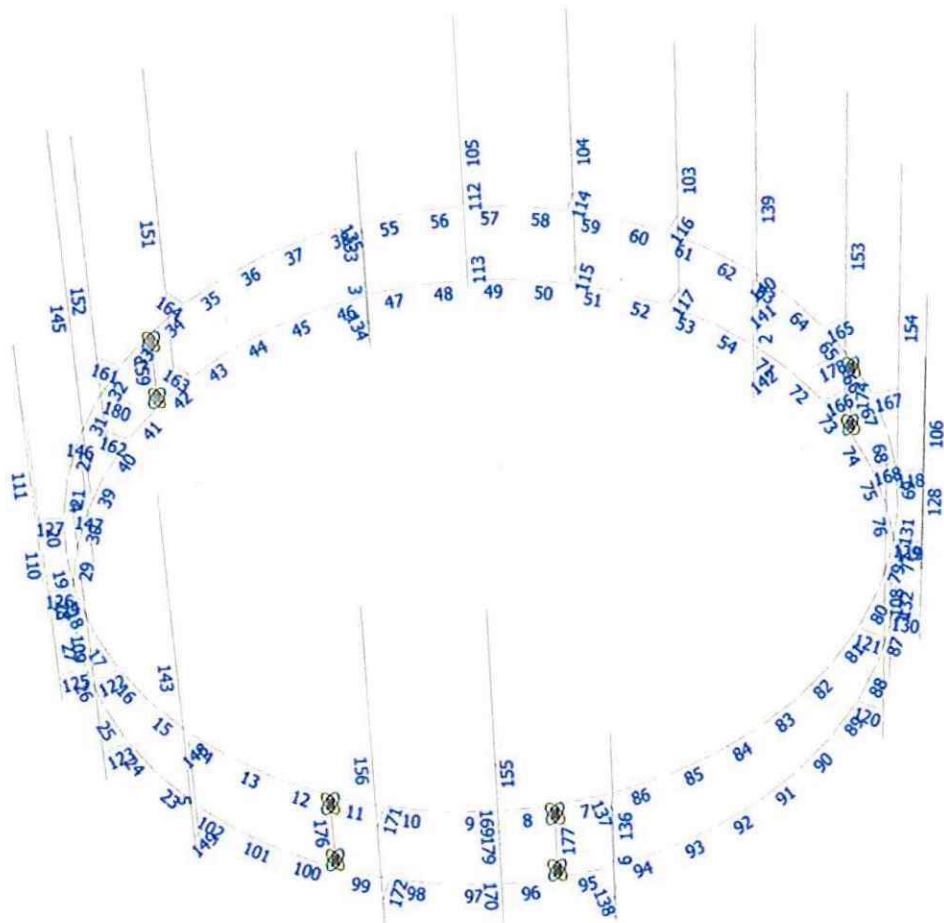
# Edge

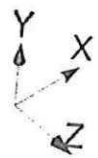
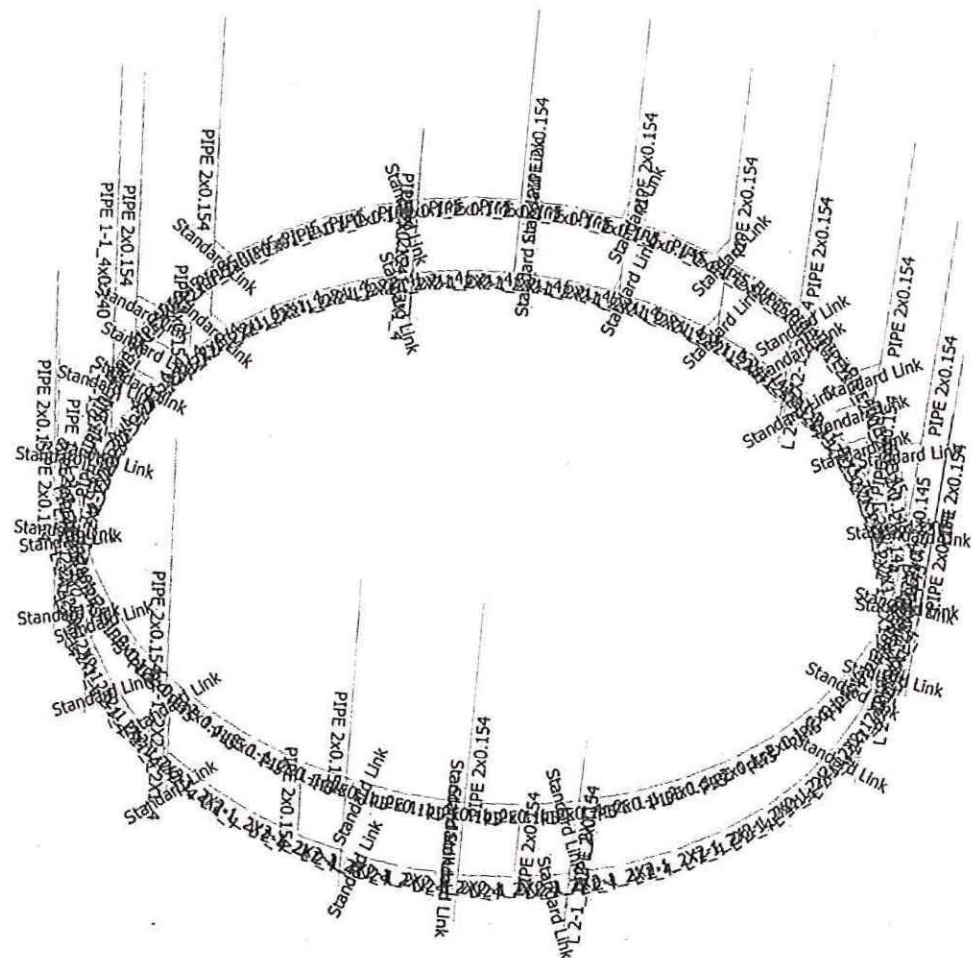
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Current Date: 11/20/2015 10:46 AM

Units system: English

File name: \\edgeex02\active\_projects\13700\13736\Structural\2015-11-20 Railing Analysis\RAM\Cambridge WT 13736 Railing Evaluation\_2015-11-20.etz\







# Edge

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Current Date: 11/20/2015 10:52 AM

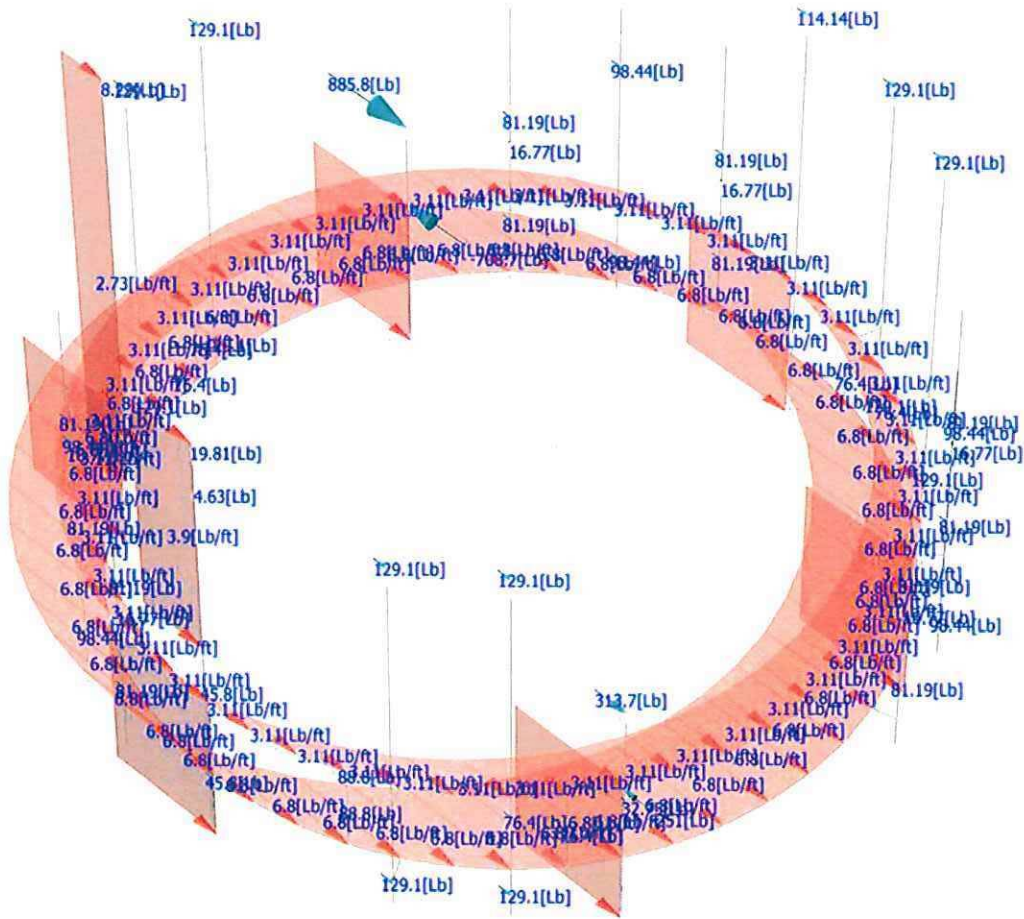
Units system: English

File name: \edgeex02\active\_projects\13700\13736\Structural\2015-11-20 Railing Analysis\RAM\Cambridge WT\_13736\_Railing Evaluation\_2015-11-20.etz\

Load condition: WLz=Wind Load Z Direction

### Loads

- Global distributed - Members
- Local distributed - Members
- Concentrated - Members

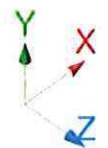
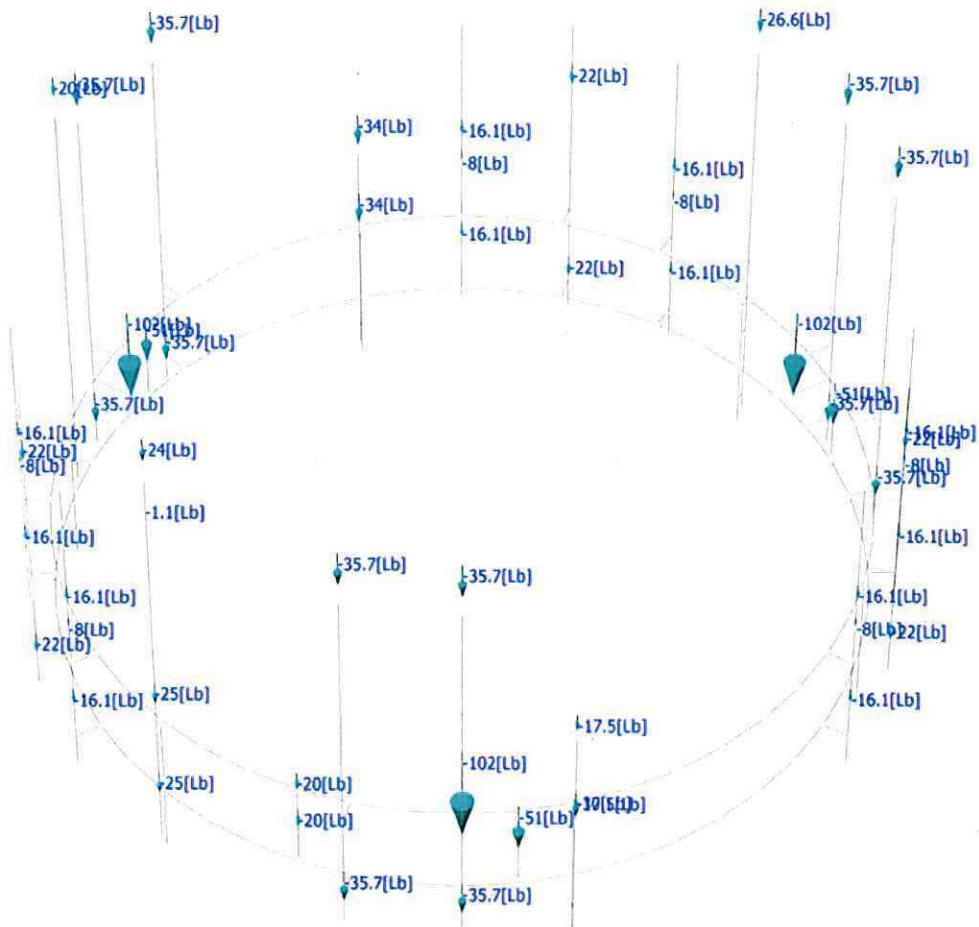






Loads

■ Concentrated - Members





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Current Date: 11/20/2015 10:56 AM

Units system: English

File name: \\edgeex02\active\_projects\13700\13736\Structural\2015-11-20 Railing Analysis\RAM\Cambridge WT\_13736\_Railing Evaluation\_2015-11-20.etz\

## Steel Code Check

Report: Summary - Group by member

Load conditions to be included in design :

D1=DL  
 D2=DL+Wlx  
 D3=DL+0.866Wlx+0.5WLz  
 D4=DL+0.707Wlx+0.707WLz  
 D5=DL+0.5Wlx+0.866WLz  
 D6=DL+Wlz  
 D7=DL-0.5Wlx+0.866WLz  
 D8=DL-0.707Wlx+0.707WLz  
 D9=DL-0.866Wlx+0.5WLz  
 D10=DL-Wlx  
 D11=DL-0.866Wlx-0.5WLz  
 D12=DL-0.707Wlx-0.707WLz  
 D13=DL-0.5Wlx-0.866WLz  
 D14=DL-Wlz  
 D15=DL+0.5Wlx-0.866WLz  
 D16=DL+0.707Wlx-0.707WLz  
 D17=DL+0.866Wlx-0.5WLz  
 D18=0.6DL+Wlx  
 D19=0.6DL+0.866Wlx+0.5WLz  
 D20=0.6DL+0.707Wlx+0.707WLz  
 D21=0.6DL+0.5Wlx+0.866WLz  
 D22=0.6DL+Wlz  
 D23=0.6DL-0.5Wlx+0.866WLz  
 D24=0.6DL-0.707Wlx+0.707WLz  
 D25=0.6DL-0.866Wlx+0.5WLz  
 D26=0.6DL-Wlx  
 D27=0.6DL-0.866Wlx-0.5WLz  
 D28=0.6DL-0.707Wlx-0.707WLz  
 D29=0.6DL-0.5Wlx-0.866WLz  
 D30=0.6DL-Wlz  
 D31=0.6DL+0.5Wlx-0.866WLz  
 D32=0.6DL+0.707Wlx-0.707WLz  
 D33=0.6DL+0.866Wlx-0.5WLz

Description	Section	Member	Ctrl Eq.	Ratio	Status	Reference
	<i>L 2-1_2X2-1_2X1_4</i>	1	D10 at 0.00%	3.30	N.G.	Eq. H1-1b
		2	D16 at 0.00%	2.71	N.G.	Eq. H1-1b
		3	D13 at 0.00%	2.82	N.G.	Eq. H1-1b
		4	D10 at 0.00%	2.53	N.G.	Eq. H1-1b
		5	D8 at 0.00%	2.62	N.G.	Eq. H1-1b
		6	D13 at 0.00%	1.95	N.G.	Eq. H1-1b
		23	D8 at 0.00%	1.59	N.G.	Eq. H1-1b
		24	D7 at 100.00%	0.65	OK	Eq. H1-1b
		25	D23 at 0.00%	0.71	OK	Eq. H1-1b
		26	D31 at 100.00%	0.72	OK	Eq. H1-1b
		27	D15 at 0.00%	0.85	OK	Eq. H1-1b
		28	D15 at 100.00%	0.81	OK	Eq. H1-1b
		29	D16 at 0.00%	0.83	OK	Eq. H1-1b

30	D14 at 100.00%	1.33	N.G.	Eq. H1-1b
39	D11 at 0.00%	1.09	N.G.	Eq. H1-1b
40	D11 at 100.00%	0.52	OK	Eq. H1-1b
41	D9 at 0.00%	0.38	OK	Eq. H1-1b
42	D14 at 100.00%	0.40	OK	Eq. H1-1b
43	D2 at 0.00%	1.03	N.G.	Eq. H1-1b
44	D17 at 0.00%	0.55	OK	Eq. H1-1b
45	D16 at 100.00%	0.61	OK	Eq. H1-1b
46	D16 at 100.00%	1.44	N.G.	Eq. H1-1b
47	D14 at 0.00%	1.60	N.G.	Eq. H1-1b
48	D12 at 100.00%	0.81	OK	Eq. H1-1b
49	D28 at 0.00%	1.02	N.G.	Eq. H1-1b
50	D20 at 100.00%	0.91	OK	Eq. H1-1b
51	D4 at 0.00%	1.10	N.G.	Eq. H1-1b
52	D5 at 100.00%	0.99	OK	Eq. H1-1b
53	D5 at 0.00%	0.93	OK	Eq. H1-1b
54	D3 at 100.00%	1.80	N.G.	Eq. H1-1b
71	D17 at 0.00%	1.84	N.G.	Eq. H1-1b
72	D17 at 100.00%	0.82	OK	Eq. H1-1b
73	D17 at 0.00%	0.61	OK	Eq. H1-1b
74	D2 at 100.00%	0.75	OK	Eq. H1-1b
75	D9 at 0.00%	0.68	OK	Eq. H1-1b
76	D8 at 100.00%	0.83	OK	Eq. H1-1b
77	D8 at 0.00%	0.63	OK	Eq. H1-1b
87	D3 at 0.00%	0.96	OK	Eq. H1-1b
88	D3 at 0.00%	0.47	OK	Eq. H1-1b
89	D10 at 0.00%	0.86	OK	Eq. H1-1b
90	D10 at 0.00%	0.56	OK	Eq. H1-1b
91	D10 at 0.00%	0.26	OK	Eq. H1-1b
92	D10 at 100.00%	0.35	OK	Eq. H1-1b
93	D10 at 100.00%	0.72	OK	Eq. H1-1b
94	D10 at 100.00%	1.14	N.G.	Eq. H1-1b
95	D6 at 0.00%	0.97	OK	Eq. H1-1b
96	D5 at 100.00%	0.51	OK	Eq. H1-1b
97	D9 at 100.00%	0.58	OK	Eq. H1-1b
98	D9 at 0.00%	0.58	OK	Eq. H1-1b
99	D11 at 0.00%	0.95	OK	Eq. H1-1b
100	D12 at 0.00%	0.62	OK	Eq. H1-1b
101	D11 at 100.00%	0.76	OK	Eq. H1-1b
102	D11 at 100.00%	1.63	N.G.	Eq. H1-1b
132	D9 at 68.75%	0.93	OK	Eq. H1-1b

PIPE 1-1\_2x0.145

7	D5 at 0.00%	0.56	OK	Eq. H1-1b
8	D2 at 100.00%	0.96	OK	Eq. H1-1b
9	D14 at 0.00%	0.86	OK	Eq. H1-1b
10	D4 at 100.00%	0.71	OK	Eq. H1-1b
11	D11 at 0.00%	1.16	N.G.	Eq. H1-1b
12	D10 at 0.00%	0.62	OK	Eq. H1-1b
13	D10 at 100.00%	0.51	OK	Eq. H1-1b
14	D13 at 100.00%	0.81	OK	Eq. H1-1b
15	D7 at 0.00%	0.78	OK	Eq. H1-1b
16	D7 at 100.00%	0.48	OK	Eq. H1-1b
17	D7 at 0.00%	0.88	OK	Eq. H1-1b
18	D15 at 100.00%	0.88	OK	Eq. H1-1b
19	D15 at 0.00%	0.92	OK	Eq. H1-1b
20	D15 at 100.00%	0.99	OK	Eq. H1-1b
21	D16 at 0.00%	0.70	OK	Eq. H1-1b
22	D15 at 100.00%	0.72	OK	Eq. H1-1b
31	D10 at 0.00%	0.60	OK	Eq. H1-1b
32	D10 at 100.00%	0.82	OK	Eq. H1-1b
33	D3 at 0.00%	0.86	OK	Eq. H1-1b
34	D10 at 100.00%	0.77	OK	Eq. H1-1b
35	D3 at 0.00%	1.10	N.G.	Eq. H1-1b

36	D2 at 0.00%	0.62	OK	Eq. H1-1b
37	D2 at 100.00%	0.59	OK	Eq. H1-1b
38	D2 at 100.00%	1.31	N.G.	Eq. H1-1b
55	D14 at 0.00%	0.94	OK	Eq. H1-1b
56	D12 at 100.00%	0.83	OK	Eq. H1-1b
57	D12 at 0.00%	1.04	N.G.	Eq. H1-1b
58	D4 at 100.00%	1.16	N.G.	Eq. H1-1b
59	D4 at 0.00%	1.08	N.G.	Eq. H1-1b
60	D4 at 100.00%	1.28	N.G.	Eq. H1-1b
61	D4 at 0.00%	0.72	OK	Eq. H1-1b
62	D4 at 100.00%	0.95	OK	Eq. H1-1b
63	D17 at 0.00%	0.77	OK	Eq. H1-1b
64	D17 at 100.00%	0.99	OK	Eq. H1-1b
65	D9 at 0.00%	0.95	OK	Eq. H1-1b
66	D17 at 100.00%	0.97	OK	Eq. H1-1b
67	D8 at 0.00%	0.95	OK	Eq. H1-1b
68	D9 at 100.00%	0.81	OK	Eq. H1-1b
69	D8 at 0.00%	0.78	OK	Eq. H1-1b
79	D2 at 0.00%	0.52	OK	Eq. H1-1b
80	D17 at 100.00%	0.34	OK	Eq. H1-1b
81	D10 at 0.00%	0.85	OK	Eq. H1-1b
82	D10 at 0.00%	0.60	OK	Eq. H1-1b
83	D9 at 0.00%	0.54	OK	Eq. H1-1b
84	D9 at 100.00%	0.59	OK	Eq. H1-1b
85	D10 at 100.00%	0.61	OK	Eq. H1-1b
86	D10 at 100.00%	0.97	OK	Eq. H1-1b
131	D9 at 68.75%	0.71	OK	Eq. H1-1b

**PIPE 1-1\_4x0.140**

145	D2 at 81.25%	0.64	With warnings	Eq. H1-1a
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**PIPE 2x0.154**

103	D5 at 14.58%	1.04	N.G.	Eq. H1-1b
104	D4 at 14.58%	1.12	N.G.	Eq. H1-1b
105	D12 at 14.58%	1.12	N.G.	Eq. H1-1b
106	D9 at 14.58%	0.86	OK	Eq. H1-1b
108	D2 at 14.58%	0.60	OK	Eq. H1-1b
109	D7 at 14.58%	0.69	OK	Eq. H1-1b
110	D15 at 14.58%	0.84	OK	Eq. H1-1b
111	D15 at 14.58%	0.98	OK	Eq. H1-1b
128	D4 at 37.50%	0.36	OK	Eq. H1-1b
133	D16 at 41.67%	2.07	N.G.	Eq. H1-1b
136	D16 at 41.67%	0.74	OK	Eq. H1-1b
139	D4 at 67.19%	0.88	OK	Eq. H1-1b
143	D4 at 66.67%	0.31	OK	Eq. H1-1b
151	D16 at 64.58%	0.86	OK	Eq. H1-1b
152	D16 at 65.63%	0.87	OK	Eq. H1-1b
153	D4 at 65.63%	0.87	OK	Eq. H1-1b
154	D16 at 64.58%	0.86	OK	Eq. H1-1b
155	D16 at 65.63%	0.87	OK	Eq. H1-1b
156	D16 at 64.58%	0.86	OK	Eq. H1-1b
159	D7 at 50.00%	0.05	OK	Eq. H1-1b
174	D4 at 50.00%	0.05	OK	Eq. H1-1b
176	D9 at 0.00%	0.21	OK	
177	D8 at 0.00%	0.16	OK	

**Standard Link**

112	D12 at 0.00%	0.01	OK	
113	D12 at 0.00%	0.01	OK	
114	D4 at 0.00%	0.01	OK	
115	D4 at 0.00%	0.01	OK	
116	D5 at 0.00%	0.01	OK	
117	D5 at 0.00%	0.01	OK	
118	D9 at 0.00%	0.01	OK	
119	D9 at 0.00%	0.01	OK	
120	D2 at 0.00%	0.00	OK	

121	D2 at 0.00%	0.00	OK	
122	D7 at 0.00%	0.01	OK	
123	D7 at 0.00%	0.01	OK	
124	D15 at 0.00%	0.01	OK	
125	D15 at 0.00%	0.01	OK	
126	D15 at 0.00%	0.01	OK	
127	D16 at 0.00%	0.01	OK	
129	D9 at 0.00%	0.00	OK	
130	D9 at 0.00%	0.00	OK	
134	D2 at 0.00%	0.00	OK	
135	D3 at 0.00%	0.01	OK	
137	D3 at 0.00%	0.00	OK	
138	D10 at 0.00%	0.00	OK	
140	D14 at 0.00%	0.01	OK	
141	D10 at 0.00%	0.00	OK	
142	D14 at 0.00%	0.00	OK	
146	D9 at 0.00%	0.00	OK	
147	D9 at 0.00%	0.00	OK	
148	D14 at 0.00%	0.00	OK	
149	D11 at 0.00%	0.00	OK	
161	D10 at 0.00%	0.01	OK	
162	D10 at 0.00%	0.00	OK	
163	D2 at 0.00%	0.00	OK	
164	D2 at 0.00%	0.01	OK	
165	D16 at 0.00%	0.01	OK	
166	D17 at 0.00%	0.01	OK	
167	D8 at 0.00%	0.01	OK	
168	D9 at 0.00%	0.00	OK	
169	D3 at 0.00%	0.01	OK	
170	D4 at 0.00%	0.00	OK	
171	D12 at 0.00%	0.01	OK	
172	D11 at 0.00%	0.00	OK	
178	D14 at 100.00%	0.00	OK	Eq. H1-1b
179	D4 at 100.00%	0.00	OK	Eq. H1-1b
180	D2 at 100.00%	0.00	OK	Eq. H1-1b

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Current Date: 11/20/2015 10:57 AM

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File name: \\edge\02\active\_projects\13700\13736\Structural\2015-11-20 Railing Analysis\RAM\Cambridge WT\_13736\_Railing Evaluation\_2015-11-20.etz

## Steel Code Check

Report: Comprehensive

Members: Hot-rolled

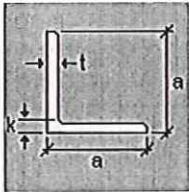
Design code: AISC 360-2005 ASD

Member : 1  
Design status : N.G.

## Section information

Section name: L 2-1\_2X2-1\_2X1\_4 (US)

### Dimensions



a = 2.500 [in] Flange length  
k = 0.500 [in] Distance k  
t = 0.250 [in] Thickness

### Properties

Section properties	Unit	Major axis	Minor axis
Gross area of the section. (Ag)	[in <sup>2</sup> ]	1.190	
Moment of Inertia (local axes) (I)	[in <sup>4</sup> ]	0.692	0.692
Moment of Inertia (principal axes) (I')	[in <sup>4</sup> ]	1.108	0.276
Bending constant for moments (principal axis) (J')	[in]	0.000	1.668
Radius of gyration (local axes) (r)	[in]	0.763	0.763
Radius of gyration (principal axes) (r')	[in]	0.965	0.482
Saint-Venant torsion constant. (J)	[in <sup>4</sup> ]	0.026	
Section warping constant. (Cw)	[in <sup>6</sup> ]	0.012	
Distance from centroid to shear center (principal axis) (xo,yo)	[in]	-0.837	-0.011
Top elastic section modulus of the section (local axis) (Ssup)	[in <sup>3</sup> ]	0.387	0.387
Bottom elastic section modulus of the section (local axis) (Sinf)	[in <sup>3</sup> ]	0.975	0.975
Top elastic section modulus of the section (principal axis) (S'sup)	[in <sup>3</sup> ]	0.633	0.304
Bottom elastic section modulus of the section (principal axis) (S'inf)	[in <sup>3</sup> ]	0.633	0.304
Plastic section modulus (local axis) (Z)	[in <sup>3</sup> ]	0.695	0.694
Plastic section modulus (principal axis) (Z')	[in <sup>3</sup> ]	0.997	0.499
Polar radius of gyration. (ro)	[in]	1.360	
Area for shear (Aw)	[in <sup>2</sup> ]	0.630	0.630
Torsional constant. (C)	[in <sup>3</sup> ]	0.099	

Material : A36

Properties	Unit	Value
Yield stress (Fy):	[Kip/in <sup>2</sup> ]	36.00
Tensile strength (Fu):	[Kip/in <sup>2</sup> ]	58.00
Elasticity Modulus (E):	[Kip/in <sup>2</sup> ]	29000.00
Shear modulus for steel (G):	[Kip/in <sup>2</sup> ]	11507.94

## DESIGN CRITERIA

Description	Unit	Value
Length for tension slenderness ratio (L)	[ft]	3.50

### Distance between member lateral bracing points

Length (Lb) [ft]	
Top	Bottom
3.50	3.50

### Laterally unbraced length

Major axis(L33)	Length [ft]		Torsional axis(Lt)	Major axis(K33)	Effective length factor	
	Minor axis(L22)				Minor axis(K22)	Torsional axis(Kt)
3.50	3.50	3.50	3.50	1.0	1.0	1.0

### Additional assumptions

Continuous lateral torsional restraint	No
Tension field action	No
Continuous flexural torsional restraint	No
Effective length factor value type	None
Major axis frame type	Sway
Minor axis frame type	Sway
Single angle connected through width	No
Planar element	No
Consider eccentricity	No
Shear load point of application	Gravity center

## DESIGN CHECKS

### AXIAL TENSION DESIGN ✓

#### Axial tension

Ratio	: 0.01	Reference	: Eq. Sec. D2
Capacity	: 25652.69 [Lb]	Ctrl Eq.	: D31 at 43.75%
Demand	: 361.30 [Lb]		

Intermediate results	Unit	Value	Reference
Factored axial tension capacity( $P_n/\phi_t$ )	[Lb]	25652.69	Eq. Sec. D2
Nominal axial tension capacity ( $P_n$ )	[Lb]	42840.00	Eq. D2-1

### AXIAL COMPRESSION DESIGN ✓

#### Compression in the major axis 33



Ratio : 0.00  
Capacity : 0.00 [Lb]  
Demand : 0.00 [Lb]      Ctrl Eq. : --

Intermediate results	Unit	Value	Reference
<u>Section classification</u>			
Unstiffened element classification	--	N/A	
Stiffened element classification	--	N/A	

**Compression in the minor axis 22**

Ratio : 0.06  
Capacity : 14506.14 [Lb]      Reference : Sec. E1  
Demand : 885.96 [Lb]      Ctrl Eq. : D7 at 0.00%

Intermediate results	Unit	Value	Reference
<u>Section classification</u>			
Unstiffened element classification	--	Non slender	
Unstiffened element slenderness ( $\lambda$ )	--	10.00	
Unstiffened element limiting slenderness ( $\lambda_r$ )	--	12.77	
Stiffened element classification	--	Non slender	
<u>Factored flexural buckling strength</u> ( $P_{n22}/\Omega$ )	[Lb]	14506.14	Sec. E1
Effective length factor (K22)	--	1.00	
Unbraced length (L22)	[ft]	3.50	
Effective slenderness ( $(KL/r)_{22}$ )	--	104.06	Eq. E5-3
Elastic critical buckling stress ( $F_{e22}$ )	[Kip/in <sup>2</sup> ]	26.43	Eq. E3-4
Reduction factor for slender unstiffened elements ( $Q_{s22}$ )	--	1.00	
Effective area of the cross section based on the effective width (A...)	[in <sup>2</sup> ]	1.19	Eq. E3-2
Reduction factor for slender stiffened elements ( $Q_{a22}$ )	--	1.00	
Full reduction factor for slender elements ( $Q_{22}$ )	--	1.00	Sec. E7
Critical stress for flexural buckling ( $F_{cr22}$ )	[Kip/in <sup>2</sup> ]	20.36	Eq. E3-2
Nominal flexural buckling strength ( $P_{n22}$ )	[Lb]	24225.26	Eq. E3-1

**FLEXURAL DESIGN**      ✕

**Bending about major axis, M33**

Ratio : 1.96  
Capacity : 0.83 [Kip\*ft]      Reference : Sec. F1  
Demand : 1.63 [Kip\*ft]      Ctrl Eq. : D10 at 0.00%

Intermediate results	Unit	Value	Reference
<u>Section classification</u>			
Unstiffened element classification	--	Compact	
Unstiffened element slenderness ( $\lambda$ )	--	10.00	
Limiting slenderness for noncompact unstiffened element ( $\lambda_r$ )	--	25.83	
Limiting slenderness for compact unstiffened element ( $\lambda_p$ )	--	15.33	
Stiffened element classification	--	Compact	
Stiffened element slenderness ( $\lambda$ )	--	10.00	
Limiting slenderness for noncompact stiffened element ( $\lambda_r$ )	--	25.83	
Limiting slenderness for compact stiffened element ( $\lambda_p$ )	--	15.33	
<u>Factored yielding strength</u> ( $M_n/\Omega$ )	[Kip*ft]	1.71	Sec. F1
Yield Moment (My)	[Kip*ft]	1.90	Sec. F10.1
Yielding (Mn)	[Kip*ft]	2.85	Eq. F10-1
<u>Factored lateral-torsional buckling strength</u> ( $M_n/\Omega$ )	[Kip*ft]	1.71	Sec. F1
Lateral-torsional buckling modification factor (Cb)	--	2.46	Eq. F1-1

Elastic lateral-torsional buckling moment (Me)	[Kip*ft]	15.51	Eq. F10-5
Lateral-torsional buckling (Mn)	[Kip*ft]	2.85	Eq. F10-3
<u>Factored yielding strength about a geometric axis(Mn/Ω)</u>	[Kip*ft]	1.04	Sec. F1
Yield Moment (My)	[Kip*ft]	1.16	Sec. F10.1
Yielding (Mn)	[Kip*ft]	1.74	Eq. F10-1
<u>Factored lateral-torsional buckling strength about a geometric axis(Mn/Ω)</u>	[Kip*ft]	0.83	Sec. F1
Lateral-torsional buckling modification factor (Cb)	--	2.60	Eq. F1-1
Elastic lateral-torsional buckling moment (Me)	[Kip*ft]	10.45	Eq. F10-4a
Lateral-torsional buckling (Mn)	[Kip*ft]	1.39	Eq. F10-3

**Bending about minor axis, M22**

Ratio	:	1.48		
Capacity	:	0.83 [Kip*ft]	Reference	: Sec. F1
Demand	:	-1.23 [Kip*ft]	Ctrl Eq.	: D3 at 0.00%

Intermediate results	Unit	Value	Reference
<u>Section classification</u>			
Unstiffened element classification	--	Compact	
Unstiffened element slenderness (λ)	--	10.00	
Limiting slenderness for noncompact unstiffened element (λ <sub>r</sub> )	--	25.83	
Limiting slenderness for compact unstiffened element (λ <sub>p</sub> )	--	15.33	
Stiffened element classification	--	Compact	
Stiffened element slenderness (λ)	--	10.00	
Limiting slenderness for noncompact stiffened element (λ <sub>r</sub> )	--	25.83	
Limiting slenderness for compact stiffened element (λ <sub>p</sub> )	--	15.33	
<u>Factored yielding strength(Mn/Ω)</u>	[Kip*ft]	0.82	Sec. F1
Yield Moment (My)	[Kip*ft]	0.91	Sec. F10.1
Yielding (Mn)	[Kip*ft]	1.37	Eq. F10-1
<u>Factored yielding strength about a geometric axis(Mn/Ω)</u>	[Kip*ft]	1.04	Sec. F1
Yield Moment (My)	[Kip*ft]	1.16	Sec. F10.1
Yielding (Mn)	[Kip*ft]	1.74	Eq. F10-1
<u>Factored lateral-torsional buckling strength about a geometric axis(Mn/Ω)</u>	[Kip*ft]	0.83	Sec. F1
Lateral-torsional buckling modification factor (Cb)	--	2.09	Eq. F1-1
Elastic lateral-torsional buckling moment (Me)	[Kip*ft]	10.45	Eq. F10-4a
Lateral-torsional buckling (Mn)	[Kip*ft]	1.39	Eq. F10-3

**DESIGN FOR SHEAR** ✓

**Shear in major axis 33**

Ratio	:	0.08		
Capacity	:	8148.50 [Lb]		
Demand	:	-639.32 [Lb]	Ctrl Eq.	: D7 at 0.00%

Intermediate results	Unit	Value	Reference
<u>Factored shear capacity(Vn/Ω)</u>	[Lb]	8148.50	
Web slenderness (λ <sub>w</sub> )	--	10.00	Sec. G2
Shear area (A <sub>w</sub> )	[in <sup>2</sup> ]	0.63	
Web buckling coefficient (k <sub>v</sub> )	--	1.20	Sec. G7
Web buckling coefficient (C <sub>v</sub> )	--	1.00	Sec. G4
Nominal shear strength (Vn)	[Lb]	13608.00	Eq. G2-1

**Shear in minor axis 22**

Ratio : 0.14  
 Capacity : 8148.50 [Lb]  
 Demand : -1105.78 [Lb]

Ctrl Eq. : D10 at 0.00%

Intermediate results	Unit	Value	Reference
<b>Factored shear capacity (<math>V_n/\Omega</math>)</b>	[Lb]	8148.50	
Web slenderness ( $\lambda_w$ )	--	10.00	Sec. G2
Shear area ( $A_w$ )	[in <sup>2</sup> ]	0.63	
Web buckling coefficient ( $k_v$ )	--	1.20	Sec. G4
Web buckling coefficient ( $C_v$ )	--	1.00	Sec. G4
Nominal shear strength ( $V_n$ )	[Lb]	13608.00	Eq. G2-1

**COMBINED ACTIONS DESIGN** X

**Combined flexure and axial compression**

Ratio : 1.61  
 Ctrl Eq. : D10 at 0.00% Reference : Eq. H1-1b

Intermediate results	Unit	Value	Reference
<b>Interaction of flexure and axial force</b>	--	1.61	Eq. H1-1b
Required flexural strength about strong axis ( $M_{r33}$ )	[Kip*ft]	1.94	
Available flexural strength about strong axis ( $M_{c33}$ )	[Kip*ft]	1.71	Sec. F1
Required flexural strength about weak axis ( $M_{r22}$ )	[Kip*ft]	-0.37	
Available flexural strength about weak axis ( $M_{c22}$ )	[Kip*ft]	0.82	Sec. F1
Required axial compressive strength ( $P_r$ )	[Lb]	483.25	
Available axial compressive strength ( $P_c$ )	[Lb]	14506.14	Sec. E1

**Combined flexure and axial tension**

Ratio : 1.59  
 Ctrl Eq. : D10 at 0.00% Reference : Eq. H1-1b

Intermediate results	Unit	Value	Reference
Required flexural strength about strong axis ( $M_{r33}$ )	[Kip*ft]	1.94	
Available flexural strength about strong axis ( $M_{c33}$ )	[Kip*ft]	1.71	Sec. F1
Required flexural strength about weak axis ( $M_{r22}$ )	[Kip*ft]	-0.37	
Available flexural strength about weak axis ( $M_{c22}$ )	[Kip*ft]	0.82	Sec. F1
Required axial tensile strength ( $P_r$ )	[Lb]	0.00	
Available axial tensile strength ( $P_c$ )	[Lb]	25652.69	Eq. Sec. D2

**Combined flexure and axial compression about local axis**

Ratio : 3.30  
 Ctrl Eq. : D10 at 0.00% Reference : Eq. H1-1b

Intermediate results	Unit	Value	Reference
Required flexural strength about strong local axis (Mr33)	[Kip*ft]	1.63	
Available flexural strength about strong local axis (Mc33)	[Kip*ft]	0.83	Sec. F1
Required flexural strength about weak local axis (Mr22)	[Kip*ft]	1.11	
Available flexural strength about weak local axis (Mc22)	[Kip*ft]	0.83	Sec. F1
Required axial compressive strength (Pr)	[Lb]	483.25	
Available axial compressive strength (Pc)	[Lb]	14506.14	Sec. E1

#### Combined flexure and axial tension about local axis

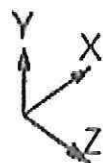
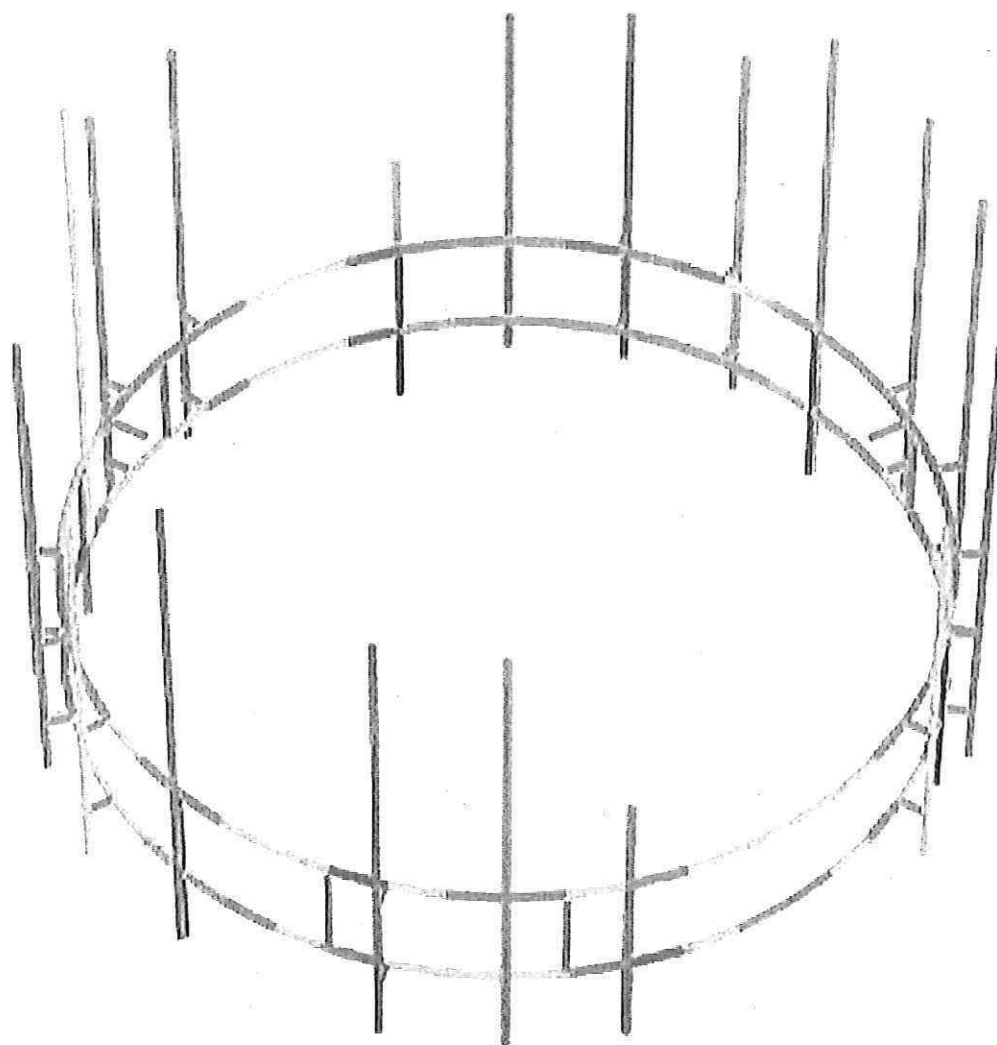
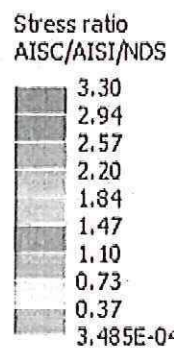
Ratio	:	3.29	Reference	:	Eq. H1-1b
Ctrl Eq.	:	D10 at 0.00%			

Intermediate results	Unit	Value	Reference
Required flexural strength about strong local axis (Mr33)	[Kip*ft]	1.63	
Available flexural strength about strong local axis (Mc33)	[Kip*ft]	0.83	Sec. F1
Required flexural strength about weak local axis (Mr22)	[Kip*ft]	1.11	
Available flexural strength about weak local axis (Mc22)	[Kip*ft]	0.83	Sec. F1
Required axial tensile strength (Pr)	[Lb]	0.00	
Available axial tensile strength (Pc)	[Lb]	25652.69	Eq. Sec. D2

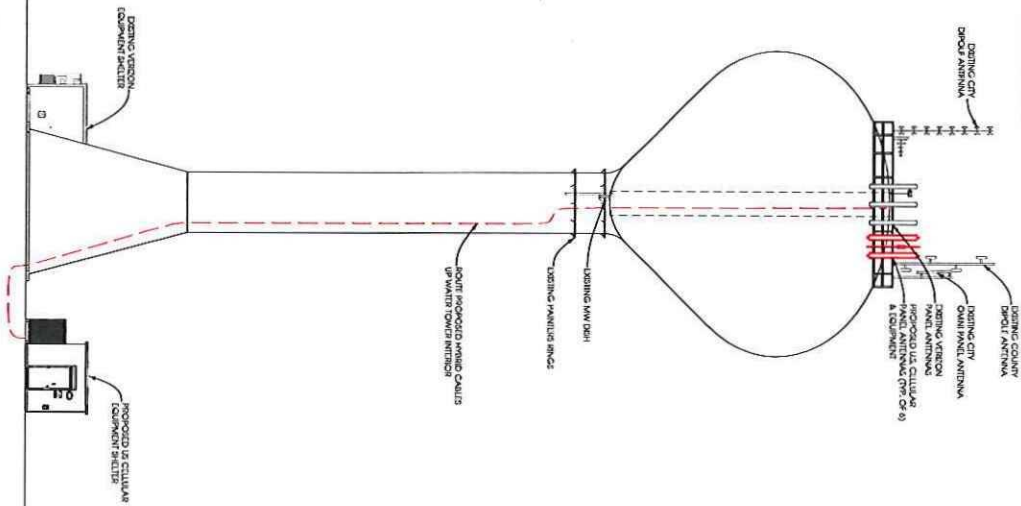
#### Combined torsion and shear stresses

Ratio	:	0.51	Reference	:	Eq. H3-8
Ctrl Eq.	:	D10 at 0.00%			

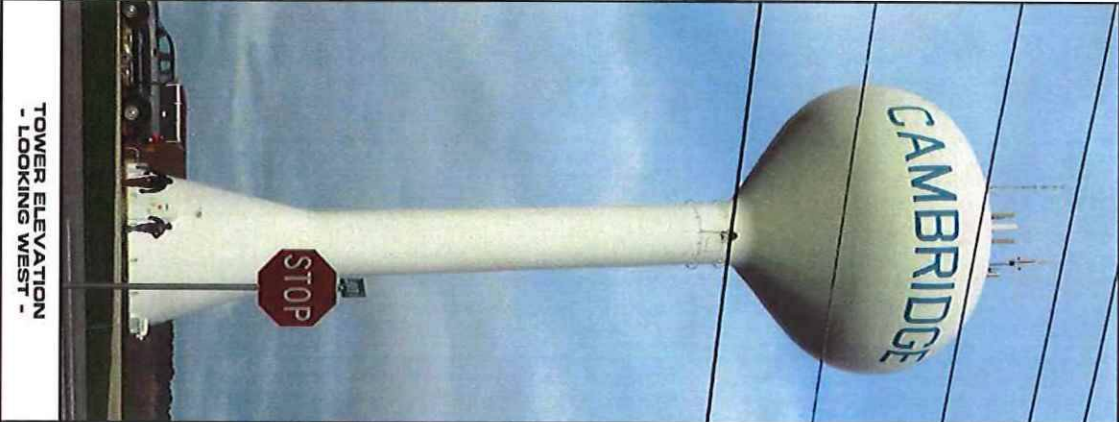
Intermediate results	Unit	Value	Reference
<u>Available shear stress for shear yielding</u> ( $F_{nv}/\Omega$ )	[Kip/in <sup>2</sup> ]	12.93	Eq. H3-8
Shear stress due to flexure in strong axis (fvb3)	[Kip/in <sup>2</sup> ]	0.66	McNulty Sec.2.3
Shear stress due to flexure in weak axis (fvb2)	[Kip/in <sup>2</sup> ]	1.76	McNulty Sec.2.3
Shear stress due to torsion (fv <sub>t</sub> )	[Kip/in <sup>2</sup> ]	4.22	DG9 T4.1
Total shear stress due to flexure and torsion (fv)	[Kip/in <sup>2</sup> ]	6.63	DG9 Sec. 4.6



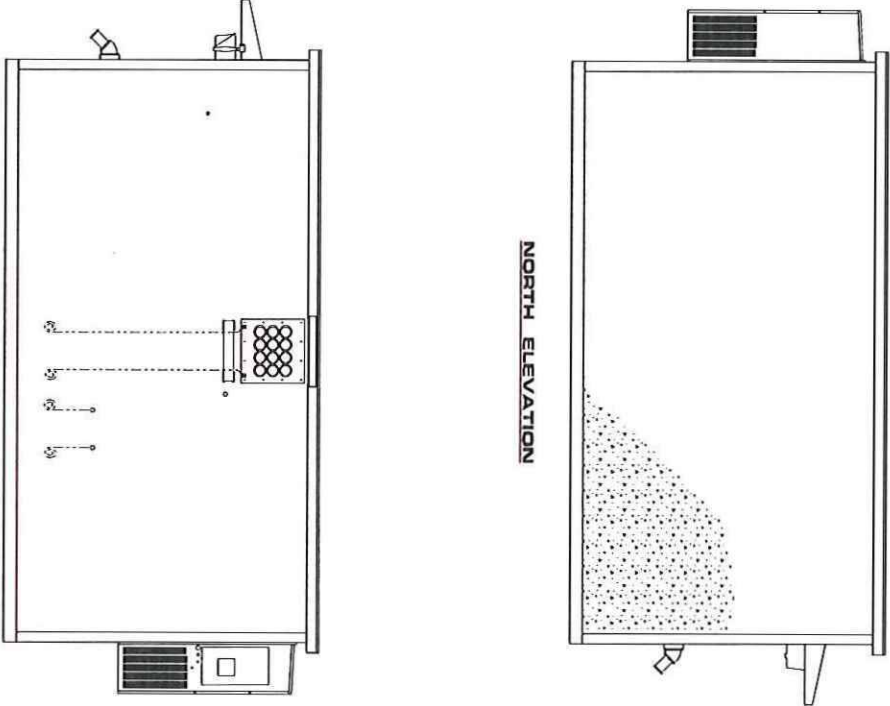
**NOTES**  
 DIMENSIONS SHOWN ARE TYPICAL AND DO NOT  
 REPRESENT ACTUAL CONDITIONS  
 CONTRACTOR TO VERIFY HEIGHT AND DIRECTION OF  
 ANTENNA WITH PROJECT MANAGER  
 ALL ANTENNA ASSUMED TO BE FROM THE NORTH



**A**  
**TOWER PROFILE (SOUTH ELEVATION)**  
 SCALE: 1/4" = 1'-0"  
 DATE: 11/11/09



**TOWER PROFILE -  
 LOOKING WEST -**



**B**  
**U.S. CELLULAR EQUIPMENT SHELTER ELEVATIONS**  
 SCALE: 1/4" = 1'-0"  
 DATE: 11/11/09

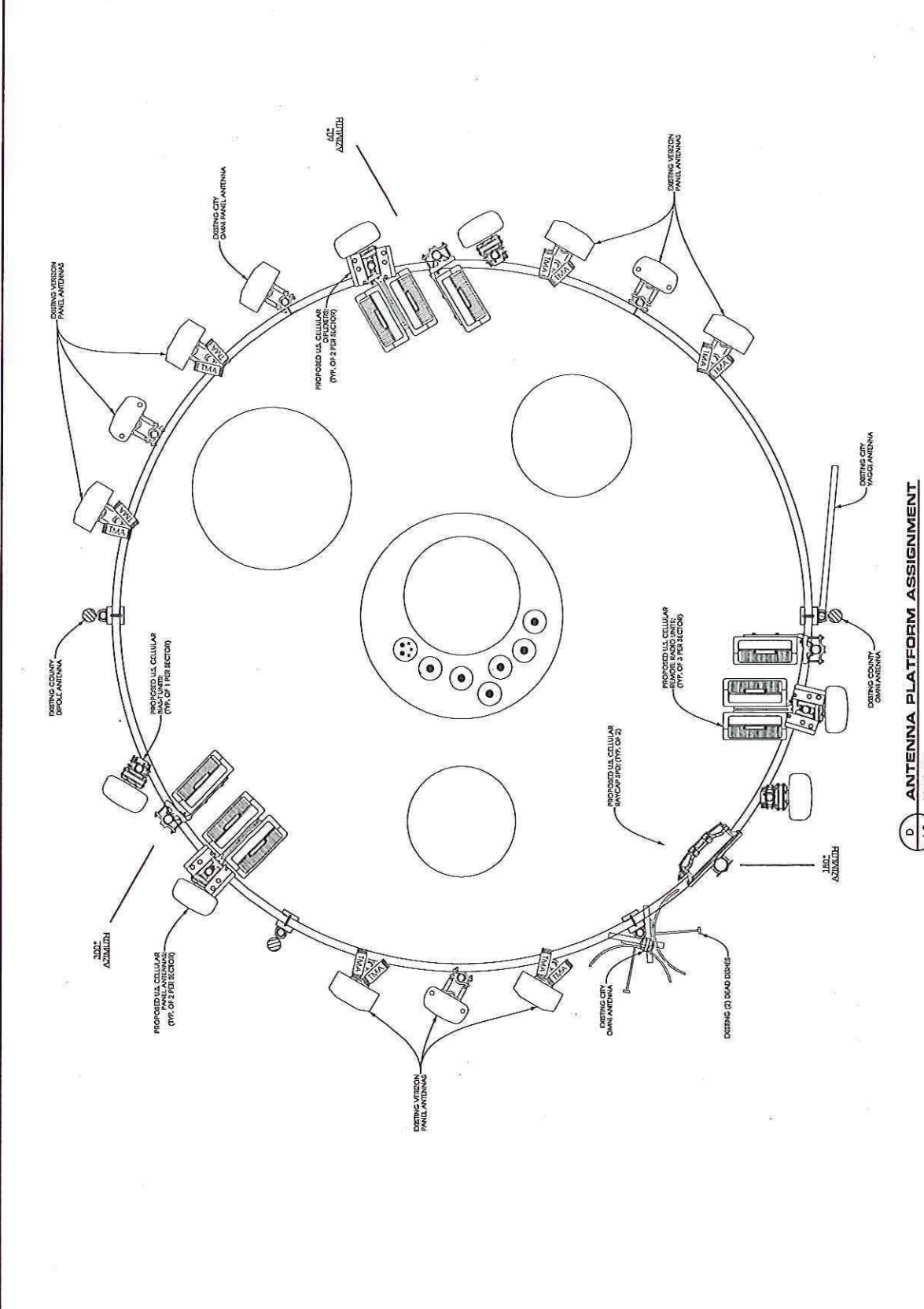
**TOWER ELEVATION  
 CAMBRIDGE WT (#782578)  
 CAMBRIDGE, WISCONSIN**

**Edge**  
 Consulting Engineers, Inc.  
 254 W. Center Street  
 Fiskeville, WI 53518  
 608-544-1545 voice  
 608-544-1547 fax  
 www.edgecons.com

DATE PLOTTED	11/11/09
DESIGNER	
CHECKED BY	
DATE	
PROJECT #	
CLIENT	
SCALE	
SHEET NUMBER	A-1
© 1998 CONSULTING ENGINEERS, INC.	

Edge Consulting Engineers, Inc.  
625 West Park Drive  
Farmingdale, NY 11737  
631-275-8000  
www.edgecorp.com

ANTENNA LAYOUT  
CAMBRIDGE, WISCONSIN  
CAMBRIDGE, WISCONSIN



D ANTENNA PLATFORM ASSIGNMENT  
SCALE: N/A

#### LEASE PARCEL

A part of the Northwest Quarter (NW1/4) of the Southeast Quarter (SE1/4) of Section One (1), Township Six (6) North, Range Twelve (12) East, Town of Christiana, Dane County, Wisconsin containing 10,000 square feet (0.229 acres) of land and being described by:

Commencing at the East Quarter Corner of said Section 1; thence S00°-21'-54"W 203.39 feet along the East line of the SE1/4 of said Section 1; thence N89°-38'-06"W 1328.14 feet to the point of beginning; thence S87°-12'-38"W 100.00 feet; thence N02°-47'-22"W 100.00 feet; thence N87°-12'-38"E 100.00 feet; thence S02°-47'-22"E 100.00 feet to the point of beginning, being subject to any and all easements and restrictions of record.

#### UTILITY AND INGRESS/EGRESS EASEMENT

A part of the Northwest Quarter (NW1/4) of the Southeast Quarter (SE1/4) of Section One (1), Township Six (6) North, Range Twelve (12) East, Town of Christiana, Dane County, Wisconsin containing 5,305 square feet (0.122 acres) of land and being described by:

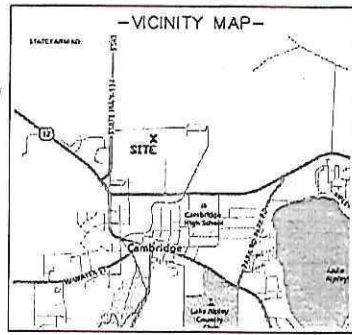
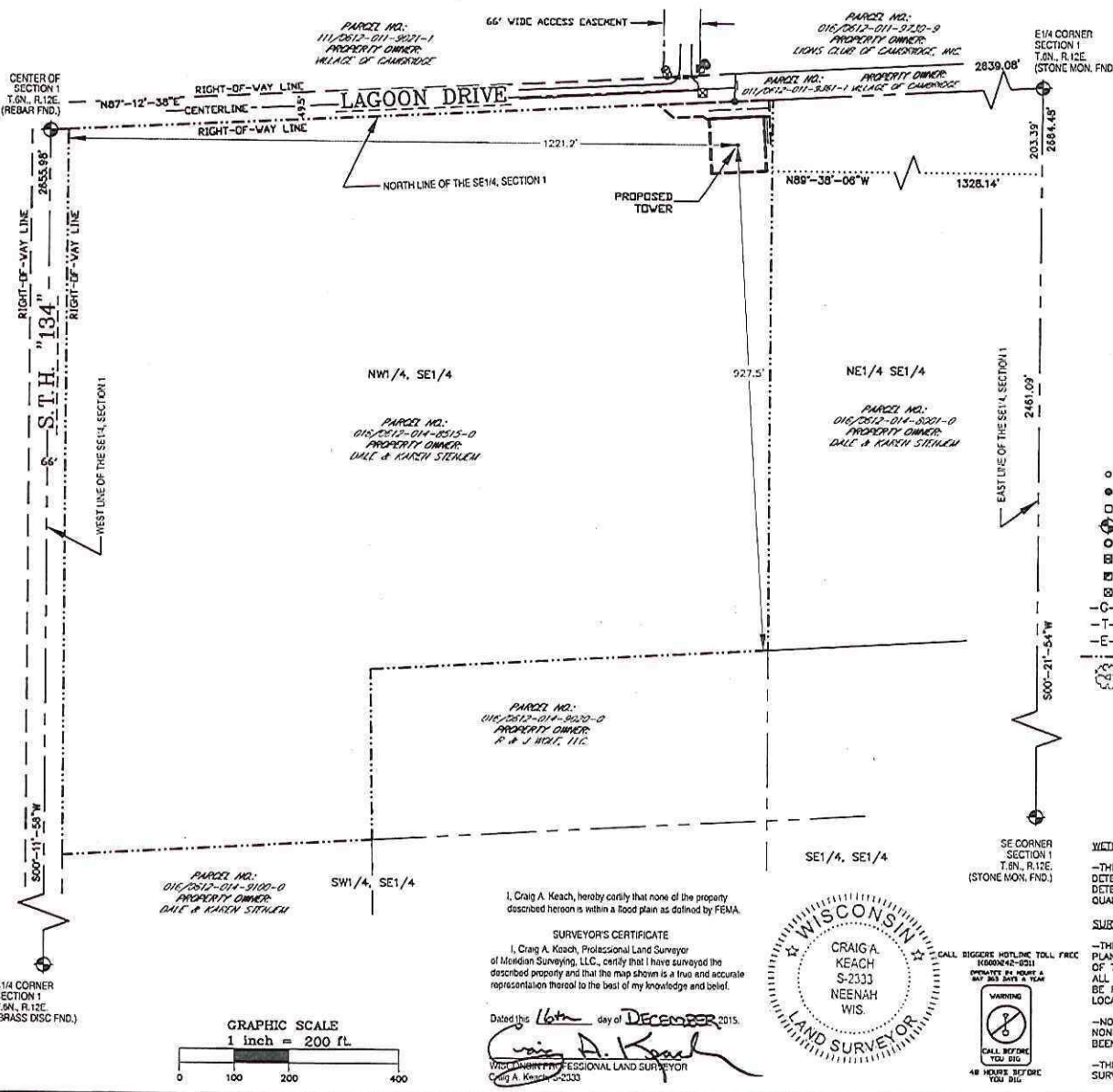
Commencing at the East Quarter Corner of said Section 1; thence S00°-21'-54"W 203.39 feet along the East line of the SE1/4 of said Section 1; thence N89°-38'-06"W 1328.14 feet; thence S87°-12'-38"W 100.00 feet; thence N02°-47'-22"W 100.00 feet to the point of beginning; thence S87°-12'-38"W 4.88 feet; N56°-46'-36"W 7.77 feet; thence S87°-58'-42"W 54.10 feet; thence N49°-55'-54"W 36.32 feet to a point on the South Right of Way line of Lagoon Drive; thence N87°-12'-38"E 201.88 feet along said South Right of Way line of Lagoon Drive; S02°-47'-22"E 30.00 feet; thence S87°-12'-38"W 110.00 feet to the point of beginning, being subject to any and all easements and restrictions of record.

#### 10 FOOT WIDE UTILITY EASEMENT

A part of the Northwest Quarter (NW1/4) of the Southeast Quarter (SE1/4) of Section One (1), Township Six (6) North, Range Twelve (12) East, Town of Christiana, Dane County, Wisconsin containing 500 square feet (0.011 acres) of land and being described by:

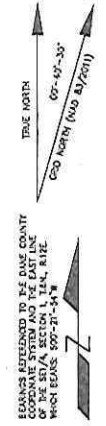
Commencing at the East Quarter Corner of said Section 1; thence S00°-21'-54"W 203.39 feet along the East line of the SE1/4 of said Section 1; thence N89°-38'-06"W 1328.14 feet; thence N02°-47'-22"W 49.97 feet to the point of beginning; thence continue thence N02°-47'-22"W 50.03 feet; thence N87°-12'-38"E 10.00 feet; S02°-47'-22"E 50.03 feet; thence S87°-12'-38"W 10.00 feet to the point of beginning, being subject to any and all easements and restrictions of record.





**PROPOSED TOWER BASE**  
 LATITUDE: 43°-00'-53.55"  
 LONGITUDE: 89°-01'-03.62"  
 (Per North American Datum of 83/2011)  
 Ground Elevation: 847.0'  
 (Per North American Vertical Datum of 1988)

- LEGEND-**
- = 1" X 18" IRON PIPE SET
  - = 1" IRON PIPE FOUND
  - = 6" NAIL SET
  - = COUNTY MONUMENT FOUND
  - = WOOD POST
  - ⊠ = ELECTRIC METER
  - ⊠ = TELEPHONE PEDESTAL
  - ⊠ = ELECTRIC TRANSFORMER
  - = BURIED GAS
  - T- = BURIED TELEPHONE
  - E- = BURIED ELECTRIC
  - - - = PROPERTY LINE
  - ⊗ = EXISTING TREE



**WETLAND NOTE:**  
 -THE PRESENCE AND LOCATION OF WETLANDS HAS NOT BEEN DETERMINED ON THIS PROPERTY. WETLANDS SHOULD ONLY BE DETERMINED BY ACTUAL FIELD DELINEATION PERFORMED BY A QUALIFIED WETLAND SPECIALIST.

**SURVEY NOTES:**  
 -THE LOCATION OF THE EXISTING UTILITIES, AS SHOWN ON THIS PLAN, ARE APPROXIMATE ONLY. IT SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR TO VERIFY ACTUAL LOCATION AND DEPTH OF ALL EXISTING UTILITIES. THE OWNER AND THE SURVEYOR SHALL NOT BE RESPONSIBLE FOR ANY OMISSION OR VARIATION FROM THE LOCATION SHOWN.  
 -NO TITLE SEARCH FOR PARCEL OWNERSHIP OR EXISTENCE OR NONEXISTENCE OF RECORDED OR UNRECORDED EASEMENTS HAS BEEN COMPLETED AS PART OF THIS SURVEY.  
 -THIS IS NOT A BOUNDARY SURVEY OF THE PARENT PARCEL. THIS SURVEY REPRESENTS THE LEASE AREA AND EASEMENTS ONLY.

SURVEYED FOR:  
  
 624 Water Street  
 Prairie du Sac, WI 53578  
 608.644.1449 voice  
 608.644.1549 fax  
 www.edgeconsult.com

SURVEYED FOR:  
  
 8410 BRYN MAWR AVENUE  
 CHICAGO, IL 60631

**MERIDIAN**  
**SURVEYING, LLC**  
 N8774 Firlane 1 Office: 920-903-0881  
 Menasha, WI 54952 Fax: 920-273-6037

**SITE NAME:** CAMBRIDGE WT - STENJEM  
**SITE NUMBER:** 782578  
**SITE ADDRESS:** 3012 S.T.H. "134"  
 CAMBRIDGE, WI 53523

**PROPERTY OWNER:** DALE & KAREN STENJEM  
 3012 S.T.H. "134"  
 CAMBRIDGE, WI 53523  
**PARCEL NO.:** 016/0612-014-8515-0  
**ZONED:** A-3  
**DEED:** VOLUME 29198, PAGE 44  
 DOCUMENT NO.: 2655527

**LEASE EXHIBIT**  
 FOR  
**US CELLULAR**  
 BEING A PART OF THE NW1/4 OF THE SE1/4, SECTION 1, T.6N., R.12E., TOWN OF CHRISTIANA, DANE COUNTY, WISCONSIN

NO.	DATE	DESCRIPTION	BY
2	12/15/15	Added Lease and Easements	J.D.
1	12/11/14	Preliminary Survey	J.D.

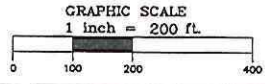
  

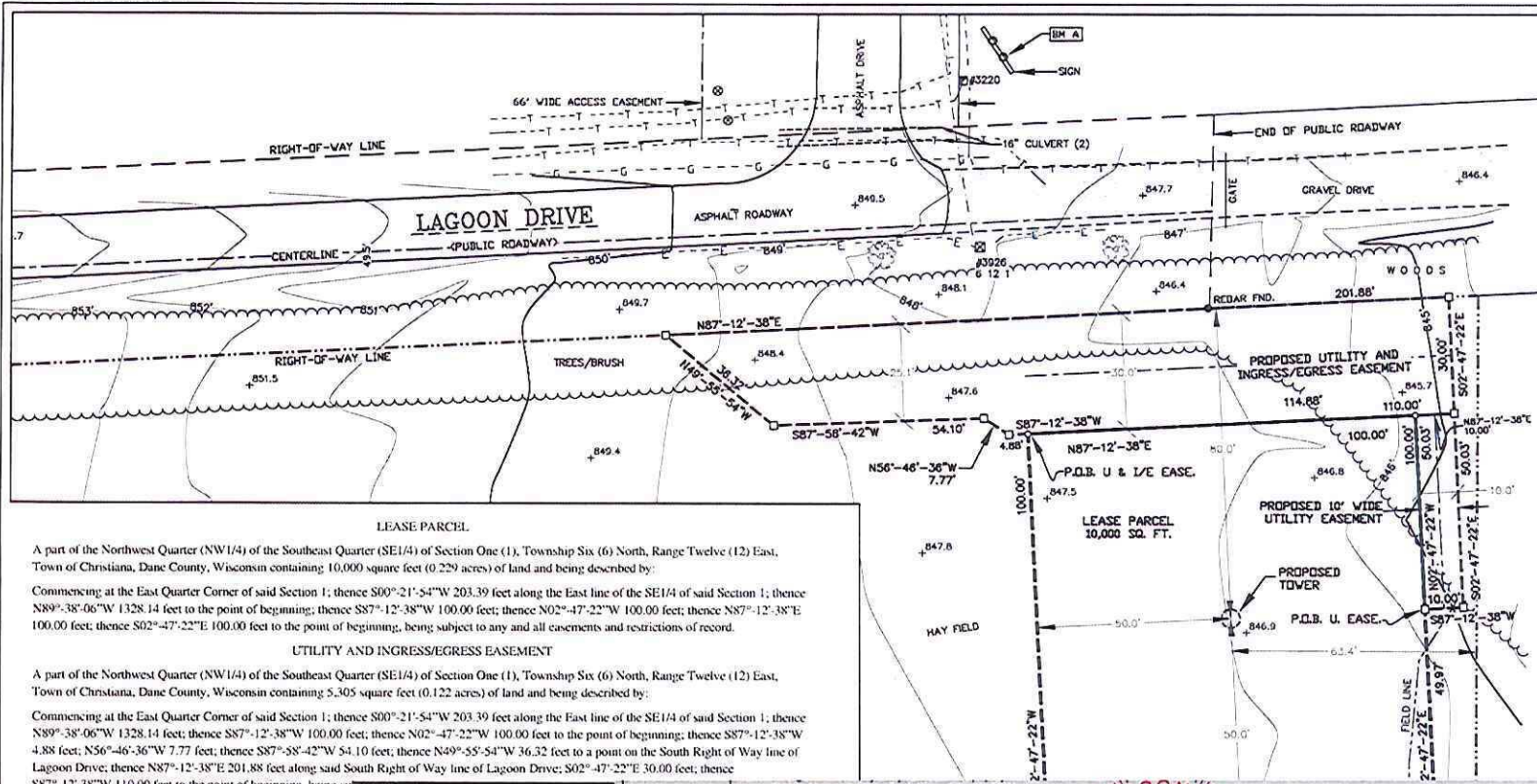
<b>DRAWN BY:</b> J.D.	<b>FIELD WORK DATE:</b> 12-8-14
<b>CHECKED BY:</b> C.A.K.	<b>FIELD BOOK:</b> M-31, PG. 69
<b>JOB NO.:</b> 8018-B1340 <b>SHEET 1 OF 2</b>	

**SURVEYOR'S CERTIFICATE**  
 I, Craig A. Keach, Professional Land Surveyor of Meridian Surveying, LLC, certify that I have surveyed the described property and that the map shown is a true and accurate representation thereof to the best of my knowledge and belief.  
 Dated this 16th day of December, 2015.  
  
 Craig A. Keach  
 Wisconsin Professional Land Surveyor  
 CRAIG A. KEACH 20333



CALL BIGGER HOTLINE TOLL FREE  
 (800) 424-0231  
 OPERATE ALL HOUR  
 800 424-0231  
  
 CALL BEFORE YOU DIG  
 48 HOURS BEFORE YOU DIG





**LEASE PARCEL**

A part of the Northwest Quarter (NW1/4) of the Southeast Quarter (SE1/4) of Section One (1), Township Six (6) North, Range Twelve (12) East, Town of Christiana, Dane County, Wisconsin containing 10,000 square feet (0.229 acres) of land and being described by:  
 Commencing at the East Quarter Corner of said Section 1; thence S00°-21'-54\"/>

**UTILITY AND INGRESS/EGRESS EASEMENT**

A part of the Northwest Quarter (NW1/4) of the Southeast Quarter (SE1/4) of Section One (1), Township Six (6) North, Range Twelve (12) East, Town of Christiana, Dane County, Wisconsin containing 5,305 square feet (0.122 acres) of land and being described by:  
 Commencing at the East Quarter Corner of said Section 1; thence S00°-21'-54\"/>

SURVEYED FOR:  
  
 Consulting Engineers, Inc.  
 624 Water Street  
 Plover du Soc, WI 53578  
 608.644.1449 voice  
 608.644.1549 fax  
 www.edgeconsult.com

SURVEYED FOR:  
  
 U.S. Cellular  
 8410 BRYN MAWR AVENUE  
 CHICAGO, IL 60631

**MERIDIAN**  
 SURVEYING, LLC  
 N8774 Firestone 1 Office: 920-993-0881  
 Menasha, WI 54952 Fax: 920-273-6037

SITE NAME: CAMBRIDGE WT - STENJEM  
 SITE NUMBER: 782578  
 SITE ADDRESS: 3012 S.T.H. "134"  
 CAMBRIDGE, WI 53523

PROPERTY OWNER:  
 DALE & KAREN STENJEM  
 3012 S.T.H. "134"  
 CAMBRIDGE, WI 53523  
 PARCEL NO.: 016/0612-014-8515-0  
 ZONED: A-3

UTILITY MONUMENT FOUND  
 D POST  
 TRIC METER  
 TRIC PEDESTAL  
 TRIC TRANSFORMER  
 ED GAS  
 ED TELEPHONE  
 ED ELECTRIC  
 PERTY LINE  
 TING TREE

BEARS REFERENCED TO THE DANE COUNTY PLAT SYSTEM AND THE EAST QUARTER CORNER OF SECTION 1, T6N, R. 12E, BEARS: S00°-21'-54\"/>

NO.	DATE	DESCRIPTION	BY
2	12/15/15	Added Lease and Easements	J.D.
1	12/11/14	Preliminary Survey	J.D.

DRAWN BY: J.D. FIELD WORK DATE: 12-8-14  
 CHECKED BY: G.A.K. FIELD BOOK: N-71, PG. 48

described herein is within a flood plain as defined by FEMA.

**SURVEYOR'S CERTIFICATE**  
 I, Craig A. Keach, Professional Land Surveyor of Meridian Surveying, LLC, certify that I have surveyed the described property and that the map shown is a true and accurate representation thereof to the best of my knowledge and belief.

Dated this 11th day of December 2015  
  
 WISCONSIN PROFESSIONAL LAND SURVEYOR

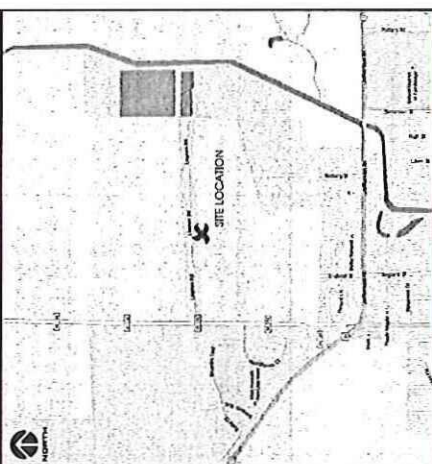
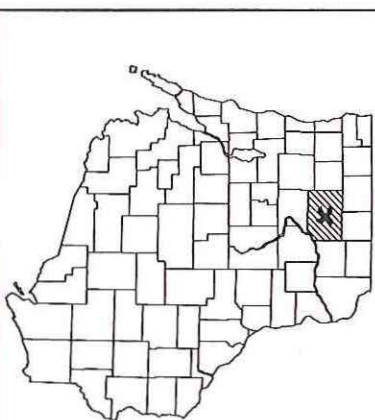


- BENCHMARK INFORMATION**  
 SITE BENCHMARK: (BM A)  
 SET 6" NAIL IN EASTERLY FACE OF 6"x6" WOOD POST FOR CAMBRIDGE LIONS CLUB SIGN; +1' ABOVE GROUND LEVEL
- = COU
  - = WOO
  - = ELEC
  - = TELE
  - = ELEC
  - C = BUR
  - T = BUR
  - E = BUR
  - = PRO
  - = EXIS

ELEVATION: 545.95'



**CAMBRIDGE STENJEM [#782578]  
CAMBRIDGE, WISCONSIN  
ZONING DRAWINGS  
195' SELF-SUPPORT TOWER  
NOVEMBER 2015**



**SITE LOCATION MAPS**



DATE	11/20/2015
DRAWN BY	JAM
CHECKED BY	
DATE	
PROJECT #	
DATE	
FILE NAME	
DATE	
SHEET NUMBER	
<b>T-1</b>	

**PROJECT INFO:**

SITE LOCATION:  
3012 S.W. 13th  
CAMBRIDGE, WI 53623

SITE #: 782578

PROPERTY OWNER:  
DALE & MARION STENJEM  
11727 WEST TERRACE DRIVE  
MADISON, WI 53718

CLIENT:  
U.S. CELLULAR - MADISON  
817 WEST TERRACE DRIVE  
MADISON, WI 53718  
CONTACT: MIKE BALISTRERI  
PHONE: 608-272-3008

2C INFORMATION (NAD 1983 (91))  
TOWER BASE - (CENTER OF TOWER)

LAT: \_\_\_\_\_  
LONG: \_\_\_\_\_  
GROUND ELEVATION (NGVD 29): \_\_\_\_\_

PLS. INFORMATION:  
PART OF NW 1/4 OF THE SE 1/4  
SECTION 1, T.2N., R.12E.,  
TOWN OF CHRISTIANA,  
DADE COUNTY,  
WISCONSIN

TAX NUMBER: 014/091201448150

**PROJECT DIRECTORY:**

ENGINEERING COMPANY:  
EDGE CONSULTING ENGINEERS, INC.  
654 WATER STREET  
PRAIRIE DU SAC, WI 53078  
CONTACT: DAVID LUSHEK  
PHONE: 608-644-1449

CLIENT:  
U.S. CELLULAR - MADISON  
817 WEST TERRACE DRIVE  
MADISON, WI 53718  
CONTACT: MIKE BALISTRERI  
PHONE: 608-272-3008

SITE ACQUISITION:  
MERIDIAN SURVEYING, LLC  
2000 WISCONSIN AVENUE  
MEMPHIS PARKS, WI 53061  
CONTACT: TODD ANDERSON  
PHONE: 414-308-2866

SURVEYOR:  
MERIDIAN SURVEYING, LLC  
2000 WISCONSIN AVENUE  
MEMPHIS PARKS, WI 53061  
CONTACT: CRAIG KEACH  
PHONE: 920.993.0881

<b>SHEET INDEX:</b>	
<b>NO.:</b>	<b>PAGE TITLE:</b>
T-1	TITLE SHEET
T-1	SITE SURVEY *
C-1	SITE PLAN
C-2	COMPOUND PLAN
A-1	TOWER ELEVATION

**UTILITY INFORMATION**

ELECTRIC SERVICE PROVIDER: ALLIANT PHONE: 800.662.6222

TELEPHONE SERVICE PROVIDER: VERIZON PHONE: \_\_\_\_\_

TO OBTAIN LOCATION OF PARTICIPANT'S UNDERGROUND FACILITIES BEFORE YOU DIG IN WISCONSIN, CALL DIGITEST HOTLINE

TOLL FREE: 1-800-4-A-DIGITEST  
FAX A LOCATE: 800.533.8468

**ENGINEER SEAL:**

PRELIMINARY - NOT FOR CONSTRUCTION

I HEREBY CERTIFY THAT THIS PLAN SET WAS PREPARED BY ME OR UNDER MY DIRECT SUPERVISION OTHER THAN THE EXCEPTIONS NOTED IN THE SHEET INDEX AND THAT I AM A DULY LICENSED PROFESSIONAL ENGINEER UNDER THE LAWS OF THE STATE OF WISCONSIN.

Signature: \_\_\_\_\_  
Date: \_\_\_\_\_

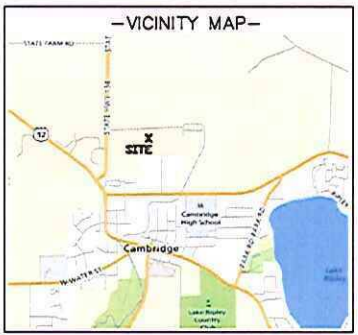
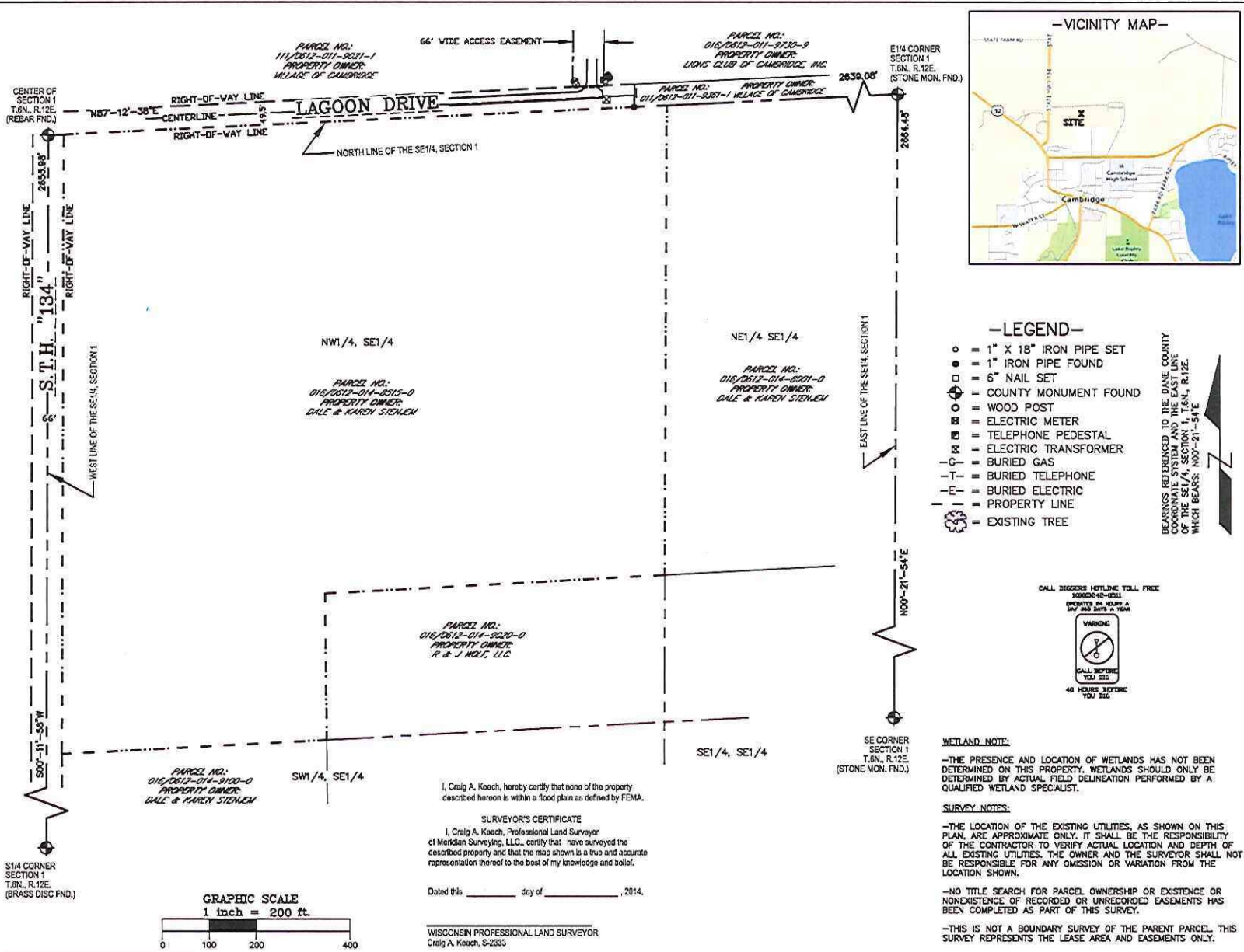
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Signature: \_\_\_\_\_  
Date: \_\_\_\_\_

\* PREPARED BY OTHERS



- LEGEND-**
- = 1" X 18" IRON PIPE SET
  - = 1" IRON PIPE FOUND
  - = 6" NAIL SET
  - ⊙ = COUNTY MONUMENT FOUND
  - ⊕ = WOOD POST
  - ⊖ = ELECTRIC METER
  - ⊗ = TELEPHONE PEDESTAL
  - ⊠ = ELECTRIC TRANSFORMER
  - ⊘ = BURIED GAS
  - T- = BURIED TELEPHONE
  - E- = BURIED ELECTRIC
  - = PROPERTY LINE
  - ⊗ = EXISTING TREE
- BEARINGS REFERENCED TO THE DANE COUNTY COORDINATE SYSTEM AND THE EAST LINE OF THE SE1/4, SECTION 1, T.6N., R.12E., WHICH BEARS N00°-21'-54"E



**WETLAND NOTE:**  
 -THE PRESENCE AND LOCATION OF WETLANDS HAS NOT BEEN DETERMINED ON THIS PROPERTY. WETLANDS SHOULD ONLY BE DETERMINED BY ACTUAL FIELD DELINEATION PERFORMED BY A QUALIFIED WETLAND SPECIALIST.

**SURVEY NOTES:**  
 -THE LOCATION OF THE EXISTING UTILITIES, AS SHOWN ON THIS PLAN, ARE APPROXIMATE ONLY. IT SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR TO VERIFY ACTUAL LOCATION AND DEPTH OF ALL EXISTING UTILITIES. THE OWNER AND THE SURVEYOR SHALL NOT BE RESPONSIBLE FOR ANY OMISSION OR VARIATION FROM THE LOCATION SHOWN.

-NO TITLE SEARCH FOR PARCEL OWNERSHIP OR EXISTENCE OR NONEXISTENCE OF RECORDED OR UNRECORDED EASEMENTS HAS BEEN COMPLETED AS PART OF THIS SURVEY.

-THIS IS NOT A BOUNDARY SURVEY OF THE PARENT PARCEL. THIS SURVEY REPRESENTS THE LEASE AREA AND EASEMENTS ONLY.

SURVEYED FOR:

624 Water Street  
 Paire du Sac, WI 53578  
 608.644.1440 voice  
 608.644.1549 fax  
 www.edgeconsult.com

SURVEYED FOR:

8410 BRYN MAWR AVENUE  
 CHICAGO, IL 60631

**MERIDIAN**  
 SURVEYING, LLC

N8774 Firelane 1 Office: 920-993-0881  
 Menasha, WI 54952 Fax: 920-273-6037

SITE NAME: CAMBRIDGE WT - STENJEM  
 SITE NUMBER: 782578  
 SITE ADDRESS:  
 3012 S.T.H. "134"  
 CAMBRIDGE, WI 53523

PROPERTY OWNER:  
 DALE & KAREN STENJEM  
 3012 S.T.H. "134"  
 CAMBRIDGE, WI 53523

PARCEL NO.: 016/0612-014-8515-0  
 ZONED: A-3  
 DEED: VOLUME 29198, PAGE 44  
 DOCUMENT NO.: 2655527

**LEASE EXHIBIT**  
 FOR  
**US CELLULAR**  
 BEING A PART OF THE NW1/4 OF THE SE1/4, SECTION 1, T.6N., R.12E., TOWN OF CHRISTIANA, DANE COUNTY, WISCONSIN

NO.	DATE	DESCRIPTION	BY
1	12/11/14	Preliminary Survey	J.D.

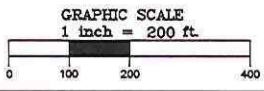
DRAWN BY: J.D. FIELD WORK DATE: 12-8-14  
 CHECKED BY: C.A.K. FIELD BOOK: M-31, PG. 69  
 JOB NO.: 8018-B1340 SHEET 1 OF 3

I, Craig A. Kauch, hereby certify that none of the property described hereon is within a flood plain as defined by FEMA.

**SURVEYOR'S CERTIFICATE**  
 I, Craig A. Kauch, Professional Land Surveyor of Meridian Surveying, LLC, certify that I have surveyed the described property and that the map shown is a true and accurate representation thereof to the best of my knowledge and belief.

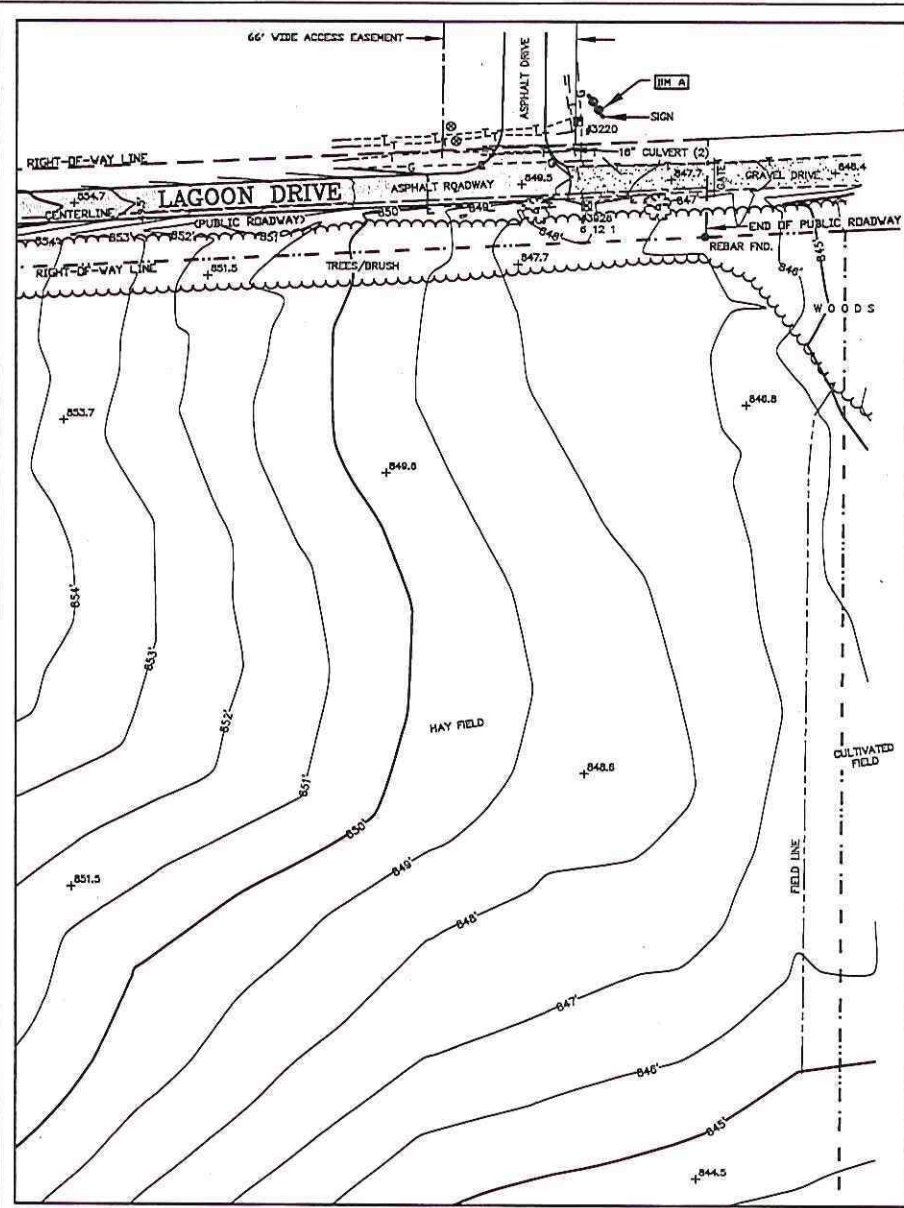
Dated this \_\_\_\_\_ day of \_\_\_\_\_, 2014.

WISCONSIN PROFESSIONAL LAND SURVEYOR  
 Craig A. Kauch, S-2333



S114 CORNER SECTION 1 T.6N., R.12E. (BRASS DISC FND.)

SE CORNER SECTION 1 T.6N., R.12E. (STONE MON. FND.)



**BENCHMARK INFORMATION**  
 SITE BENCHMARK: (BM A)  
 SET 6" NAIL IN EASTERLY FACE OF 6"X6" WOOD POST FOR  
 CAMBRIDGE LIONS CLUB SIGN; ±1' ABOVE GROUND LEVEL  
 ELEVATION: 848.98'

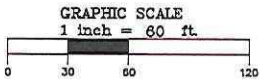
- LEGEND-**
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  - ◉ = 1" IRON PIPE FOUND
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  - ⊠ = ELECTRIC TRANSFORMER
  - ⊡ = BURIED GAS
  - ⊢ = BURIED TELEPHONE
  - ⊣ = BURIED ELECTRIC
  - ⊤ = PROPERTY LINE
  - ⊥ = EXISTING TREE

I, Craig A. Keach, hereby certify that none of the property described hereon is within a flood plain as defined by FEMA.

**SURVEYOR'S CERTIFICATE**  
 I, Craig A. Keach, Professional Land Surveyor of Meridian Surveying, LLC, certify that I have surveyed the described property and that the map shown is a true and accurate representation thereof to the best of my knowledge and belief.

Dated this \_\_\_\_\_ day of \_\_\_\_\_, 2014.

WISCONSIN PROFESSIONAL LAND SURVEYOR  
 Craig A. Keach, S-2333



BEARINGS REFERENCED TO THE DANE COUNTY  
 COORDINATE SYSTEM AND THE EAST LINE  
 OF THE SE1/4, SECTION 1, T6N., R.12E.,  
 WHICH BEARS N89-21-54E

SURVEYED FOR:

624 Water Street  
 Proino du Soc. WI 53378  
 608.644.1447 voice  
 608.644.1549 fax  
 www.edgeconsult.com

SURVEYED FOR:

6410 DRYN MAWR AVENUE  
 CHICAGO, IL 60631

**MERIDIAN**

**SURVEYING, LLC**  
 N8774 Firlane 1 Office: 920-993-0881  
 Menasha, WI 54952 Fax: 920-273-6037

**SITE NAME:** CAMBRIDGE WT - STENJEM  
**SITE NUMBER:** 782578  
**SITE ADDRESS:**  
 3012 S.T.H. "134"  
 CAMBRIDGE, WI 53523

**PROPERTY OWNER:**  
 DALE & KAREN STENJEM  
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 CAMBRIDGE, WI 53523

**PARCEL NO.:** 016/0612-014-8515-0  
**ZONED:** A-3  
**DEED:** VOLUME 29108, PAGE 44  
 DOCUMENT NO.: 2655527

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 SE1/4, SECTION 1, T.6N., R.12E.,  
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 WISCONSIN

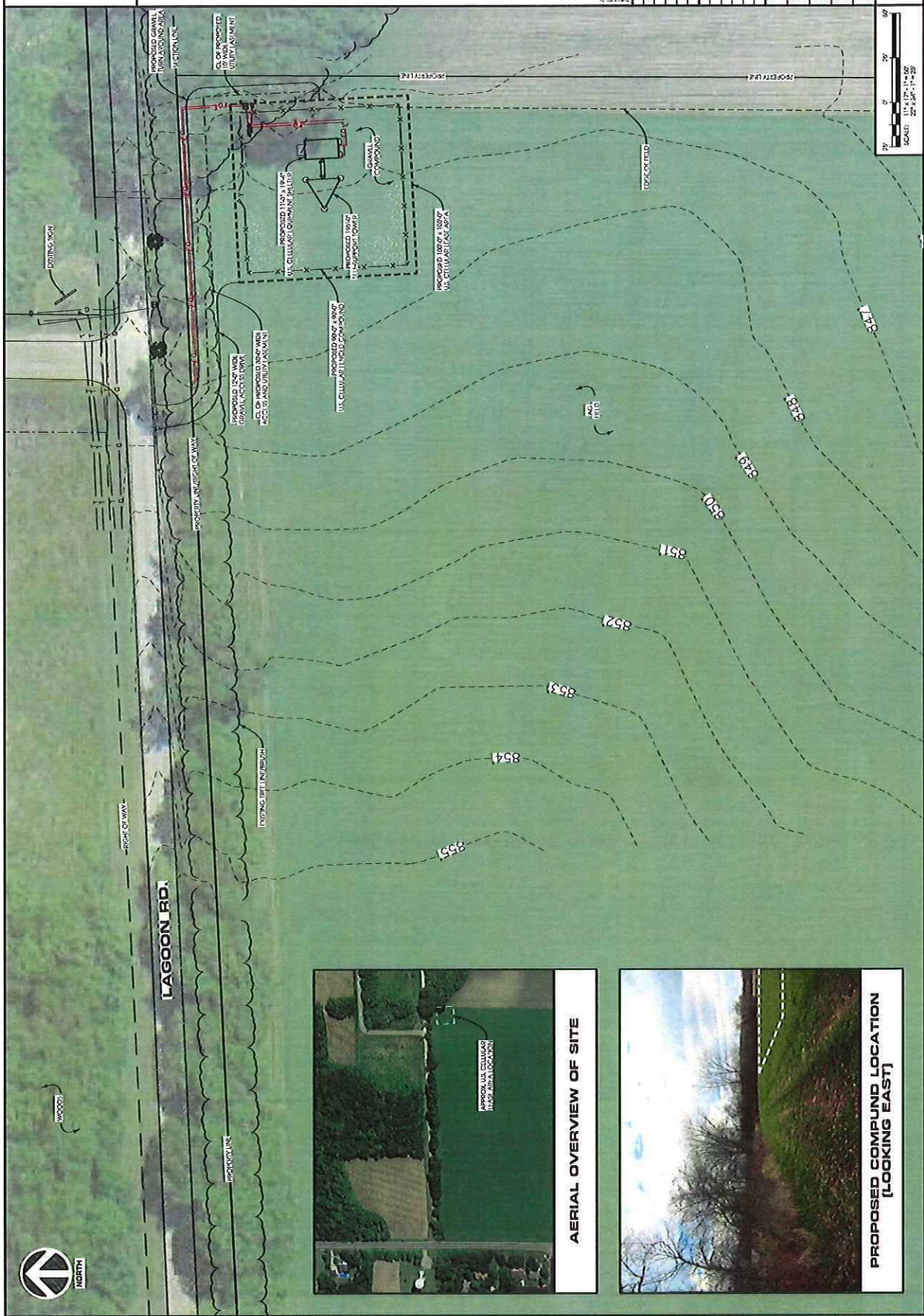
NO.	DATE	DESCRIPTION	BY
1	12/11/14	Preliminary Survey	J.D.

**DRAWN BY:** J.D. **FIELD WORK DATE:** 12-8-14  
**CHECKED BY:** C.A.K. **FIELD BOOK:** M-31, PG. 69  
 JOB NO.: 8018-B1340 **SHEET 2 OF 3**

**SITE PLAN**  
**CAMBRIDGE STENJEM (#782578)**  
**CAMBRIDGE, WISCONSIN**

DATE:	11/26/2013
DESIGNER:	STENJEM
CHECKED BY:	STENJEM
DATE:	11/26/2013
PROJECT:	CAMBRIDGE STENJEM
SHEET NO.:	1
TOTAL SHEETS:	1
SCALE:	AS SHOWN
DRAWN BY:	STENJEM
DATE:	11/26/2013
PROJECT:	CAMBRIDGE STENJEM
SHEET NO.:	1
TOTAL SHEETS:	1
SCALE:	AS SHOWN

**C-1**  
 SHEET NUMBER



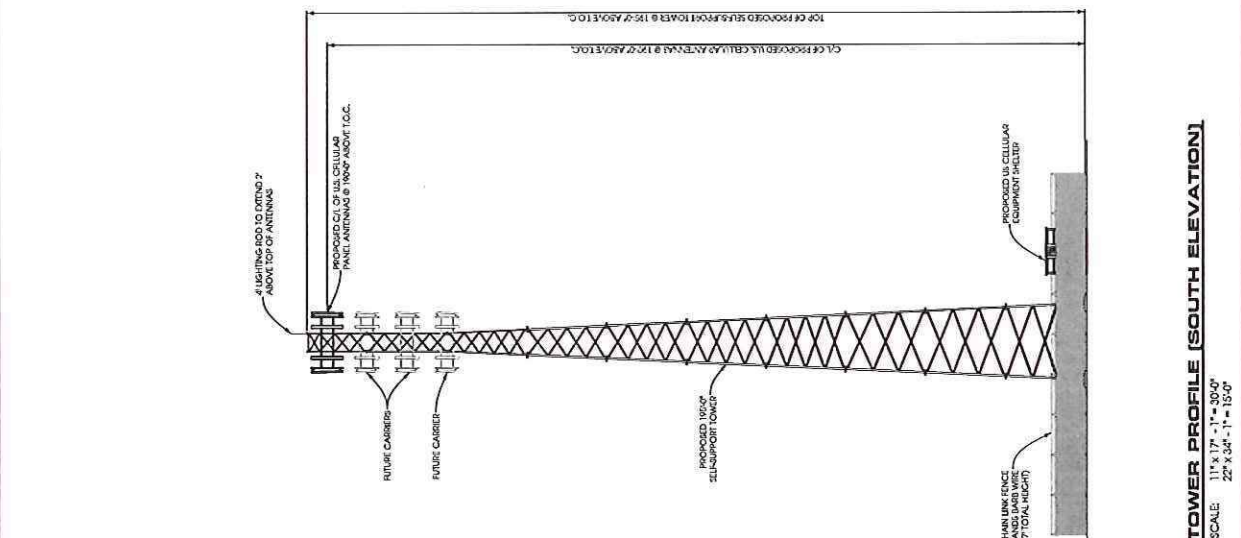
**AERIAL OVERVIEW OF SITE**



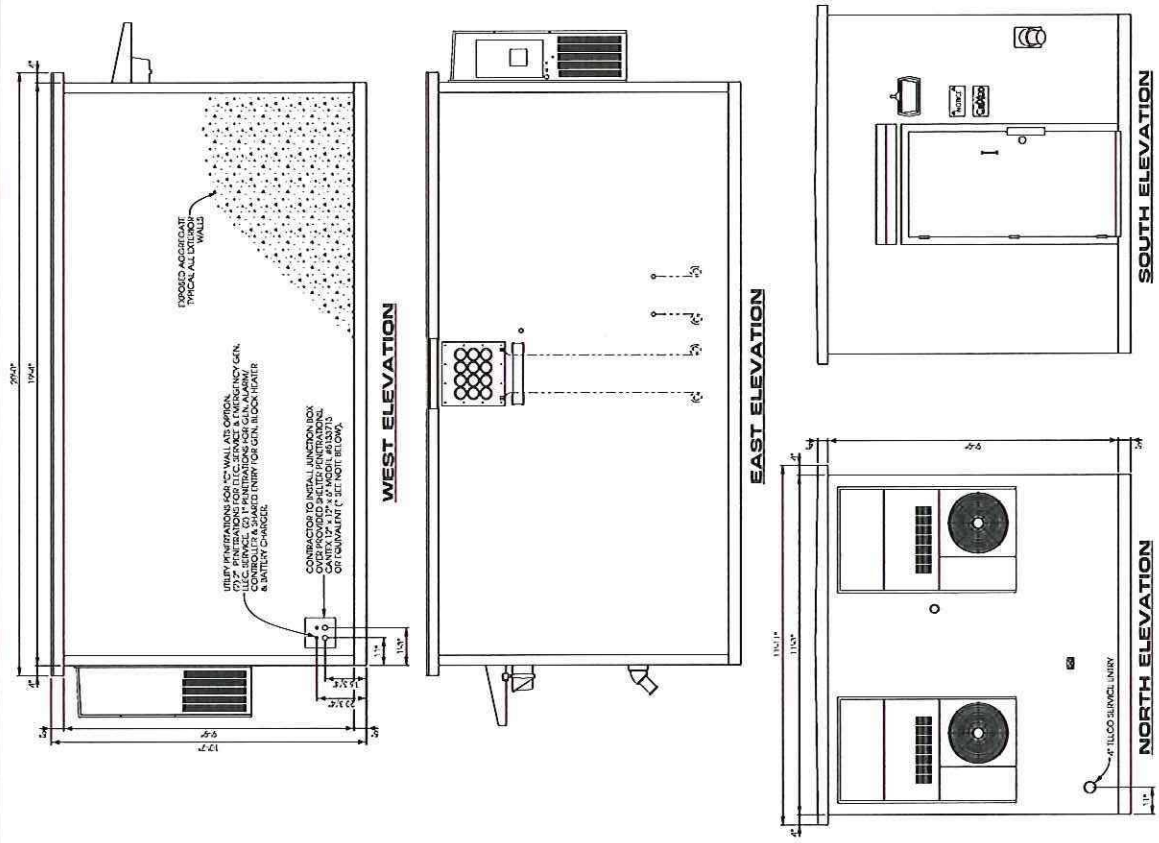
**PROPOSED COMPOUND LOCATION  
 (LOOKING EAST)**



NOTE:  
 FOUNDATIONS SHOWN ARE TYPICAL AND DO NOT  
 REPRESENT ACTUAL CONDITIONS.  
 CONTRACTOR TO VERIFY HEIGHT AND DIRECTION OF  
 ANTENNA WITH PROJECT MANAGER.  
 ALL ANTENNA ADJUSTING TO BE FROM BLUE NORTH



**A** TOWER PROFILE (SOUTH ELEVATION)  
 SCALE: 1/4" = 1'-0"  
 22' x 34' - 1" = 15'-0"



**B** EQUIPMENT SHELTER ELEVATIONS  
 SCALE: 1/4" = 1'-0"  
 22' x 34' - 1/2" = 1'-0"

**Edge** Consulting Engineers, Inc.  
 621 West Street  
 Foshay Tower, Suite 1100  
 65254-1571 MN  
 www.edgecorp.com

**TOWER ELEVATION**  
**CAMBRIDGE STENJEM (#782578)**  
**CAMBRIDGE, WISCONSIN**

DATE	1/22/2015
DESIGNED BY	AM/ML
CHECKED BY	ML
PROJECT #	11725010
PROJECT NAME	11725010
SHEET NUMBER	A-1











**RECEIPT**

MADISON  
MADISON  
210 MARTIN LUTHER KING, JR. BLVD  
CITY TREASURER OFFICE

**Application:** DCPCUP-2016-02343  
**Application Type:** DaneCounty/Zoning/Conditional Use/NA  
**Address:** 3012 STATE HIGHWAY 134, TOWN OF CHRISTIANA, WI 53523

**Receipt No.** 750092

Payment Method	Ref Number	Amount Paid	Payment Date	Cashier ID	Received	Comments
Check	1252	\$3,000.00	04/08/2016	HJH3		

**Owner Info.:** DALE L STENJEM  
3012 STATE HIGHWAY 134  
CAMBRIDGE, WI 53523

**Work Description:** 195' cell tower proposed by US Cellular